



Council for Geoscience

**A GEOPHYSICAL AND SEDIMENT SAMPLING SURVEY OF TWO
PROPOSED SAND WINNING AREAS IN THE DURBAN BIGHT**

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Durban

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1. INTRODUCTION

The Marine Geoscience Unit was contracted by Portnet to undertake a marine geophysical investigation of two areas identified as potential sites for sand winning. Rather than conducting a new survey, geophysical data from a recent survey in the Durban Bight undertaken in April and May of 1999 was used for the compilation of this report. A standard suite of geophysical instruments including a digital echo-sounder, 3.5 kHz sub-bottom profiler and a side-scan sonar were used for data collection during the survey. A grab sampling and sediment coring programme was conducted in May 2001 to investigate the nature of the sediments and to assess their suitability as backfill.

The aims of the geophysical investigation were to:

- Produce a bathymetric chart of the area encompassing both proposed borrow areas reduced to Mean Sea Level (MSL).
- Produce a side-scan sonar mosaic of the proposed borrow sites to show the nature of the seafloor.
- Assess unconsolidated sediment thickness in the vicinity of the proposed borrow sites.
- Collect grab samples to assess sediment distribution patterns in the area.
- Collect sediment cores at selected sites within the proposed borrow sites to assess sediment variation with depth.
- Make recommendations regarding the suitability of each of the potential borrow areas for sand winning.
- Delineate the most suitable areas for sand winning in each of the borrow sites.

2 GEOPHYSICAL INSTRUMENTATION

2.1 DGPS

A Fugro StarFix DGPS receiver was used for navigation throughout the geophysical survey. This is a 12 channel Trimble system with an update rate of 10 Hz and sub-metre precision. DGPS corrections are RTCM SC-104 Ver. 2.0 format, virtual base station solutions with an RTCM update rate of typically less than 5 seconds.

2.2 Odom Echotrac Digital Echosounder

An Odom Echotrac digital echosounder (Model 3100) with a narrow beam (9°) 210kHz transducer was used to collect bathymetric data of the seafloor. This instrument is capable of recording up to 20 data points per second in digital format whilst undertaking shallow water surveys. An event-annotated paper analogue profile is also produced as a backup to the digital data.

2.3 Klein System 2000 Side-scan Sonar

A Klein System 2000 side-scan sonar and model 2260 digital tow-fish were used to collect the sonographs. The Klein System 2000 is a dual frequency (100/500 kHz) side-scan sonar that is capable of collecting high resolution image corrected acoustic data. The Klein System 2000 incorporates a 7 Gigabyte 8 channel Exabyte tape drive which is used for digital data storage, and a 300 dpi, 256 grey shade thermal printer.

2.4 GeoPulse Sub-bottom Profiler

A GeoAcoustics GeoPulse sub-bottom profiling system was used to collect sub-bottom profiles during the geophysical survey. The sub-bottom profiling system consisted of a Model 5430A GeoPulse transmitter, a Model 5210 GeoPulse seismic receiver and an over-the-side mounted transducer array. The Model 5430A transmitter has a maximum output power of 10 kW and a operator selectable operating frequency range of 2 - 15 kHz. The amplifier has a signal to noise ratio of 20 dB at 100 dB gain, 1 kHz centre frequency and 1 kHz bandwidth. The GeoPulse receiver has an operating bandwidth of 50 Hz to 10 kHz and a user selectable sampling frequency of 4 to 24 kHz.

3. METHODOLOGY

3.1 Geophysical Survey

Geophysical data were collected along predetermined coast parallel survey lines located 150 m apart. DGPS coordinates were downloaded in real-time, onto a 486 survey notebook computer via an RS 232 serial cable such that positioning data, survey tracklines and other navigational data were continuously displayed on the computer screen using the *Navlog* software package. Bathymetric data were logged at 1 or 2 second intervals and downloaded into a spreadsheet along with navigation data.

The Klein System 2000 was used to simultaneously acquire 4 channels of digital side-scan sonar data and one auxiliary channel of sub-bottom profiling data and to store the digital data on Exabyte tape. A scan range of 100 metres was used to collect the side-scan sonographs, thereby facilitating a 50 metre overlap of adjacent swaths. The GeoPulse receiver was used to amplify and filter the seismic reflection data while the Klein System 2000 was used to digitally capture the seismic reflection data and produce event annotated analogue seismic profiles.

3.1 Grab Sampling

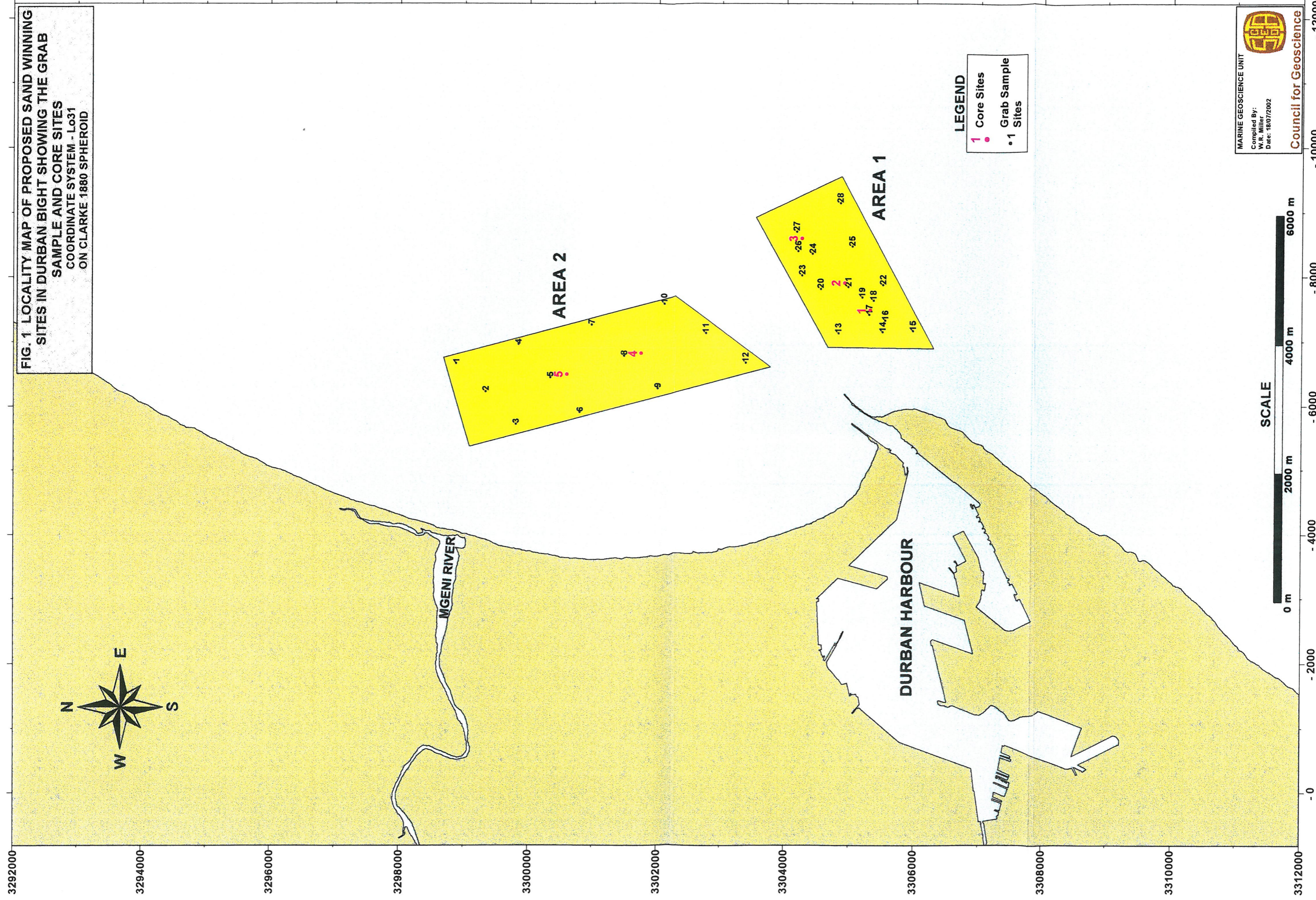
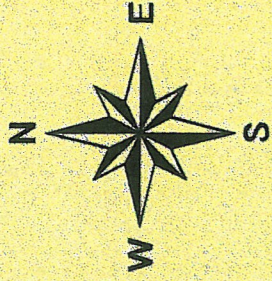
Twenty eight grab samples were collected using a *Shipek* grab, to ground-truth the side-scan sonar records obtained during April and May 1999, and also to investigate the nature of the sediments on the seafloor. The *Shipek* grab weighs ± 40 kg and takes a 0.15 m^3 sediment sample. Positioning of the grab samples was done with DGPS.

3.2 Core Sampling

Five cores measuring between 4.29 and 4.57 m were collected from the proposed borrow areas (3 from Area 1 and 2 from Area 2) to assess sediment variability with depth. The coring sites were selected by studying the sub-bottom profiling records so as to get representative sediments from both areas.

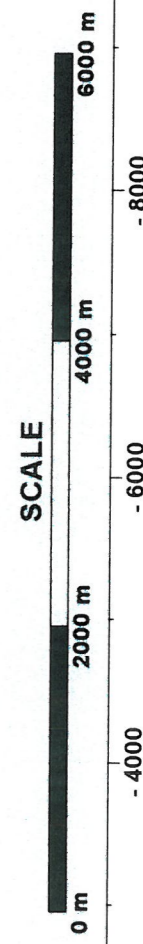
The extent of the proposed borrow sites along with grab sample and core locations are illustrated in Figure 1.

FIG. 1 LOCALITY MAP OF PROPOSED SAND WINNING SITES IN DURBAN BIGHT SHOWING THE GRAB SAMPLE AND CORE SITES ON CLARKE 1880 SPHEROID



LEGEND

- 1 Core Sites
- Grab Sample Sites



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3292000 3294000 3296000 3298000 3300000 3302000 3304000 3306000 3308000 3310000 3312000

-12000 -10000 -8000 -6000 -4000 -2000 -0

4. DATA PROCESSING

4.1 Navigation and Bathymetric Data

Navigation data were corrected for transducer offsets from the DGPS antenna position and bathymetry data were edited for anomalous values, corrected for tidal variation and reduced to Mean Sea Level (MSL) in the *Navlog Systems* software. The corrected bathymetric data were imported as ASCII text files into the *Surfer 7* software package for gridding and contouring. A total of 14379 data points were gridded using the kriging method, an octant search pattern and a search radius of 300 metres to produce a 50 m by 50 m grid file from which the final bathymetric map was produced.

4.2 Side-scan sonar data

The taped System 2000 side-scan sonar data were converted to Klein 5000 format using an Exabyte tape drive installed on a high-specification PC running Windows NT and a proprietary software application designed by Klein Associates, Inc. The Klein software allows the time varied gain (TVG) of the sonar data to be manipulated and the image enhanced. The 5KD format was then converted to Q-MIPS format using the *Navlog Systems* software. This software was also used to mosaic the sonograph data which was then filtered using an algorithm in the *ER Mapper* software. The mosaic was saved in a GeoTIFF format and imported into the *Surfer 7* software where it was geo-referenced and used to digitize different acoustic facies as separate polygons, which were integrated to produce a seafloor geology map.

4.3 Pinger sub-bottom profiling data

The navigation data were corrected for the Pinger transducer offsets in the *Navlog* software and then exported to the *Surfer 7* software as an ASCII spreadsheet. The minimum unconsolidated sediment thickness values were measured directly from the sub-bottom profiling analogue records at regularly spaced event marks (30 second intervals) and then manually incorporated into the navigation spreadsheet. These values of unconsolidated sediment thickness were then posted as point data onto the seafloor geology map in their true geographic location.

4.4 Sediment Samples

A total of 74 samples (28 grab samples & 46 samples from the sediment cores) of $\pm 130\text{g}$ each were taken for laboratory analysis. Sub-samples of the sediment were taken and dried at 100°C and then subjected to a suite of laboratory analyses. Wet sieving was undertaken to determine the mud fraction ($\% < 63 \mu\text{m}$), dry sieving was undertaken to determine the gravel fraction ($\% > 2\text{mm}$), settling tube analysis was undertaken to determine the graphic statistical parameters of the sand fraction ($63 \mu\text{m} - 2 \text{mm}$), and carbonate bomb analysis to determine calcium carbonate content. The dried sediment was poured into a 100 ml volumetric flask from a fixed height (200 mm) and weighed to determine the “loose” dry density and then subjected to 50 blows from a height of 50 mm and the new volume was measured to determine the “compact” dry density. A tabulated list of laboratory analyses is presented in Appendix 1 and cumulative frequency curves for the sand fractions are presented in Appendix 2.

4.5 Graphic Sediment Statistics

The basic descriptive element of all sediments is grain-size, which can be characterised in terms of mm or phi units (ϕ). A geometric scale was devised by Wentworth in 1922 to subdivide sediments into a number of classes based on grain-size measurements in mm. The phi unit (ϕ) is the logarithmic transformation of this scale. A number of statistical parameters can be deduced from grain-size distribution curves or directly from grain-size data, these are: mean grain-size, median grain-size, sorting and skewness. The statistical parameters are calculated using the Folk & Ward formulae given in Table 4.1 below (Folk & Ward, 1957). The statistical parameters were calculated with a BASIC based software package and a computer linked settling tube which yields results comparable to standard sieving techniques.

PARAMETER	FOLK & WARD FORMULA
Median	$Md = d_{50}$
Mean	$M = \frac{d_{16} + d_{50} + d_{84}}{3}$
Sorting	$\sigma\phi = \frac{\phi_{84} - \phi_{16}}{4} + \frac{\phi_{95} - \phi_5}{6.6}$
Skewness	$Sk = \frac{\phi_{16} + \phi_{84} - 2\phi_{50}}{2(\phi_{84} - \phi_{16})} + \frac{\phi_5 + \phi_{95} - 2\phi_{50}}{2(\phi_{95} - \phi_5)}$

Table 4.1 Formulae for the calculation of sediment grain-size parameters from grain-size data.

4.5.1 Median & Mean Grain-size

The median grain-size is simply the grain-size at 50% of the grain-size distribution, whereas the mean grain-size is an average value calculated from the 16th, 50th and 84th percentiles of the grain-size distribution (Table 4.1). These grain-size parameters are useful for subdividing sediments into a number of different classes according to the measured/calculated median or mean of a grain-size distribution (Table 4.2).

GRAIN-SIZE	ϕ VALUE	mm VALUE
Very fine-grained sand	> 3.0	0.063 to 0.125
Fine-grained sand	2.0 to 3.0	0.125 to 0.25
Medium-grained sand	1.0 to 2.0	0.25 to 0.5
Coarse-grained sand	0 to 1.0	0.5 to 1.0

Table 4.2 Grain-size scale for sand sediments.

4.5.2 Sorting

Sorting is a measure of the spread of the grain-size distribution. A well sorted sediment in terms of geological principles, is a sediment with a narrow spread of the grain-size distribution and a poorly sorted sediment is one with a broad spread of the grain-size distribution. The reverse is true when sorting is considered in terms of engineering principles i.e. a well sorted sediment has a broad grain-size distribution and a poorly sorted sediment has a narrow grain-size distribution. All references to sediment sorting in the text are made in terms of **geological** principles and are summarised in Table 4.3 below.

SORTING	ϕ VALUE
Very well sorted	< 0.35
Well sorted	0.35 to 0.5
Moderately well sorted	0.51 to 0.7
Moderately sorted	0.71 to 1.00

Table4.3 A summary of the categories of sand sorting.

4.5.3 Skewness

Skewness is the measure of the coarse or fine bias of a grain-size distribution. Apart from being useful to describe a sediment sample, skewness is also a reflection of the depositional process. In general sediment becomes more fine skewed (finer grained) along its sediment transport path whereas the source sediment (lag) becomes more coarse skewed (coarse grained) as the finer sediment is winnowed from it. The various classes of sediment skewness are summarised in Table 4.4 below.

SKEWNESS	ϕ VALUE	SURFACE AREA
Near symmetrical	-0.10 to 0.10	26.3 km ²
Coarse skewed	-0.10 to -0.30	42.7 km ²
Strongly coarse skewed	< -0.30	5.0 km ²

Table 4.4 A summary of classes of sediment skewness discussed in the text.

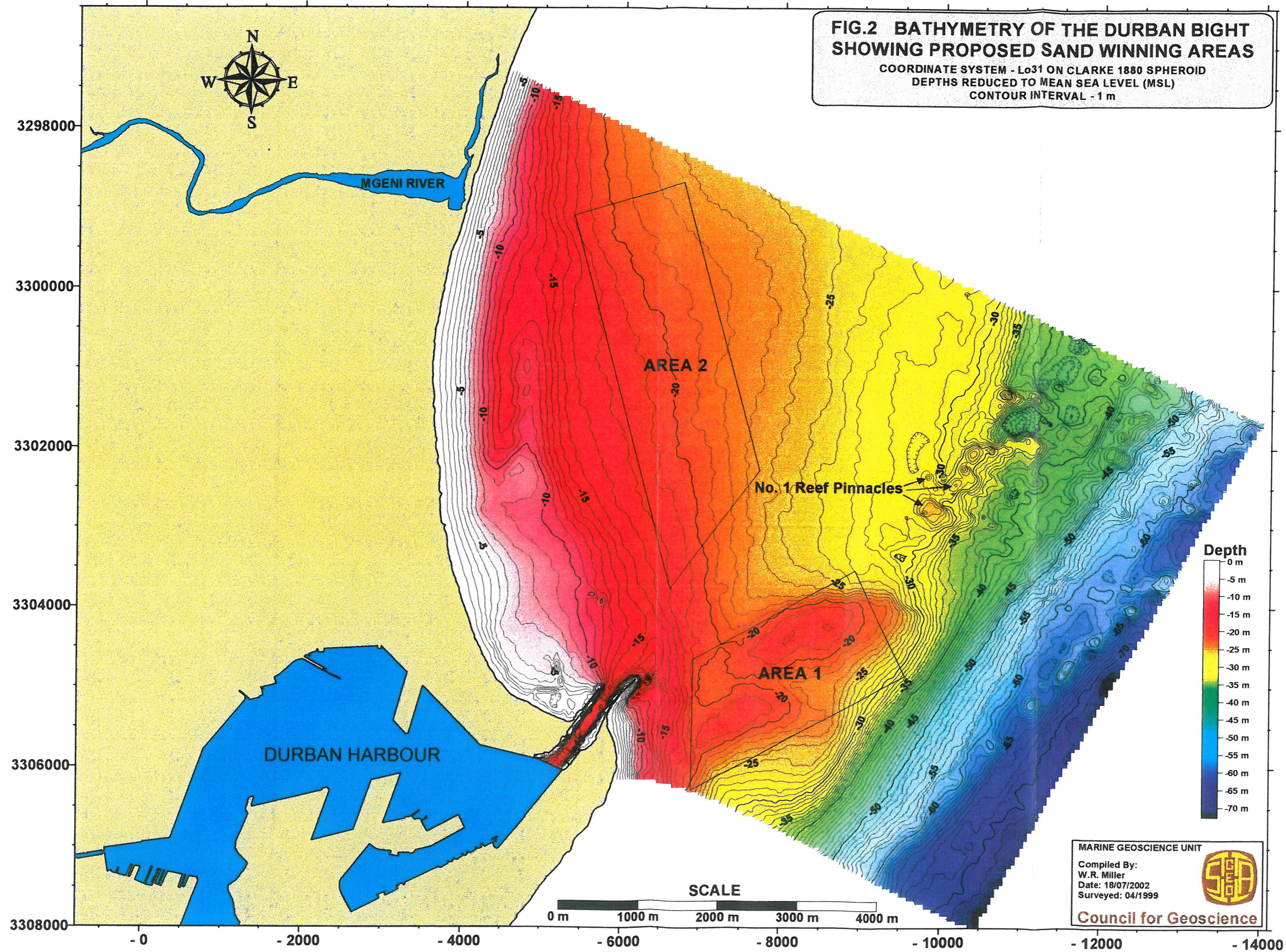
Sediment skewness is of limited importance in terms of engineering properties of sediments and this parameter receives little mention in the text. The analyses are however included in this report for sake of completeness.

5. BATHYMETRY

The bathymetry of the two borrow sites and adjacent seafloor in the Durban Bight was contoured at 1 m intervals and is illustrated in Figure 2. The bathymetry varies from a minimum depth of - 19 m to a maximum depth of -32 m in Area 1 and between - 18 m and - 23 m in Area 2 (Fig. 2). The bathymetric chart indicates that the seafloor in Area 1 is dominated by the presence of two discrete sand mounds, a northern mound which measures ± 2000 m in length, ± 750 m in width and ± 10 m in height and a southern mound which measures ± 1500 m in length, 700m in width and 2 - 3 m in height. These positive relief features are orientated roughly southwest - northeast and represent the old dredge dumping ground, which saw active dumping for 10 - 15 years during the late 1800's and early 1900's. While dumping has certainly played a role in the sea-floor morphology in this area it is unlikely that the shallow nature of the sea-floor in this area can be attributed entirely to sediment dumping. The shallow pinnacles of No. 1 Reef which are evident as a series of bullseyes defining a ridge which strikes roughly 224° to the northeast of the Area 1 borrow site, suggest that the reef may be continuous below the shallow sediment mounds in Area 1 (Fig. 2). The bathymetry is otherwise gently undulating with bathymetric gradients steepening towards the east. Bathymetric gradients vary from 0.14° in the central and western parts of Area 1 to 0.69° in the eastern part of this borrow site.

Area 2 is characterised by a very uniform bathymetry which indicates a very flat sea-floor that dips gently towards the northeast. Bathymetric gradients in Area 2 vary from 0.13° - 0.19° in northern and central areas and steepen to a maximum gradient of 0.23° further towards the south.

**FIG.2 BATHYMETRY OF THE DURBAN BIGHT
SHOWING PROPOSED SAND WINNING AREAS**
 COORDINATE SYSTEM - Lo31 ON CLARKE 1880 SPHEROID
 DEPTHS REDUCED TO MEAN SEA LEVEL (MSL)
 CONTOUR INTERVAL - 1 m



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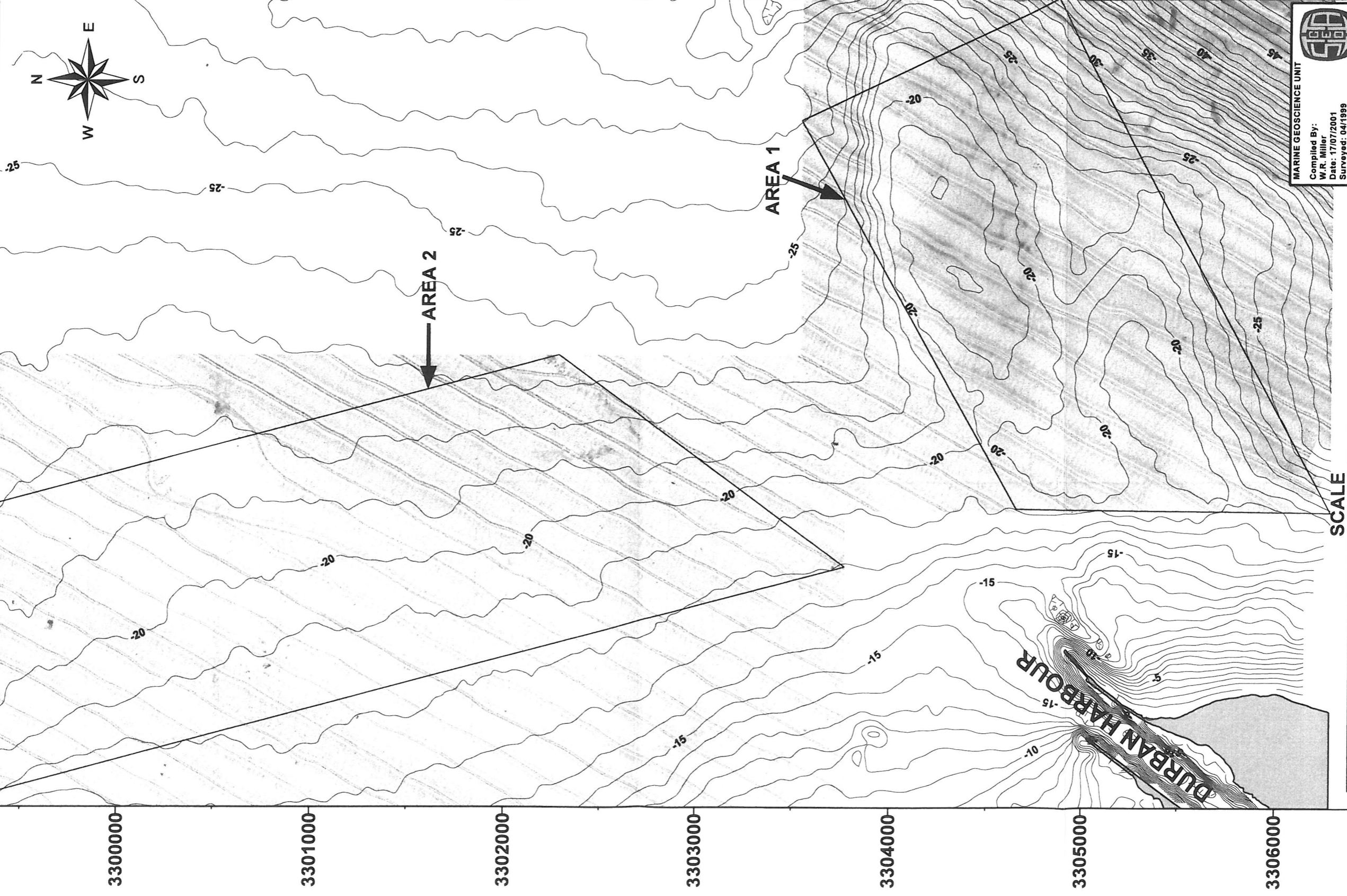
6. SURFICIAL SEAFLOOR GEOLOGY

This section deals with the geological interpretation of shelf acoustic facies interpreted from the side-scan sonar mosaic (Fig. 3). Seven acoustic facies were identified from the side-scan sonar mosaic and these include:

- A. Description: Weak to moderately reflective, smooth, even-toned planar acoustic facies.
Interpretation: Fine- to medium-grained, unconsolidated shelf sand.
- B. Description: Highly reflective acoustic facies with a scattered distribution and small acoustic shadows.
Interpretation: Scattered reef outcrop with moderate to little relief.
- C. Description: Moderate to highly reflective acoustic facies surrounded by larger patches of granular moderately reflective acoustic sediments.
Interpretation: Reef buried beneath a thin coarse-grained or bioclastic rich sediment veneer.
- D. Description: Small and localised examples of highly reflective objects with little or no acoustic shadow on the seafloor.
Interpretation: Metal debris or man-made artefacts which have been thrown overboard by passing ships.
- E. Description: Moderately to strongly reflective granular acoustic facies with a random and often linear distribution pattern.
Interpretation: Silty dredge spoil.
- F. Description: Moderately reflective acoustic facies with no shadows and diffuse irregular margins.
Interpretation: Isolated patches of marine weed growth.
- G. Description: Highly reflective, cigar-shaped object with high reflectivity and a moderate acoustic shadow.
Interpretation: Ship wreck.

The seven acoustic facies were digitised as discrete polygons and compiled to form a side-scan sonar interpretation maps for each of the proposed borrow sites (Figs. 4 & 5).

FIG. 3 SIDE-SCAN SONAR MOSAIC OF PROPOSED SAND WINNING AREAS IN DURBAN BIGHT WITH SUPERIMPOSED BATHYMETRY
COORDINATE SYSTEM - Lo31 ON CLARKE 1880 SPHEROID DEPTHS REDUCED TO MEAN SEA LEVEL (MSL) CONTOUR INTERVAL - 1 m



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Date: 17/07/2001
Surveyed: 04/1999

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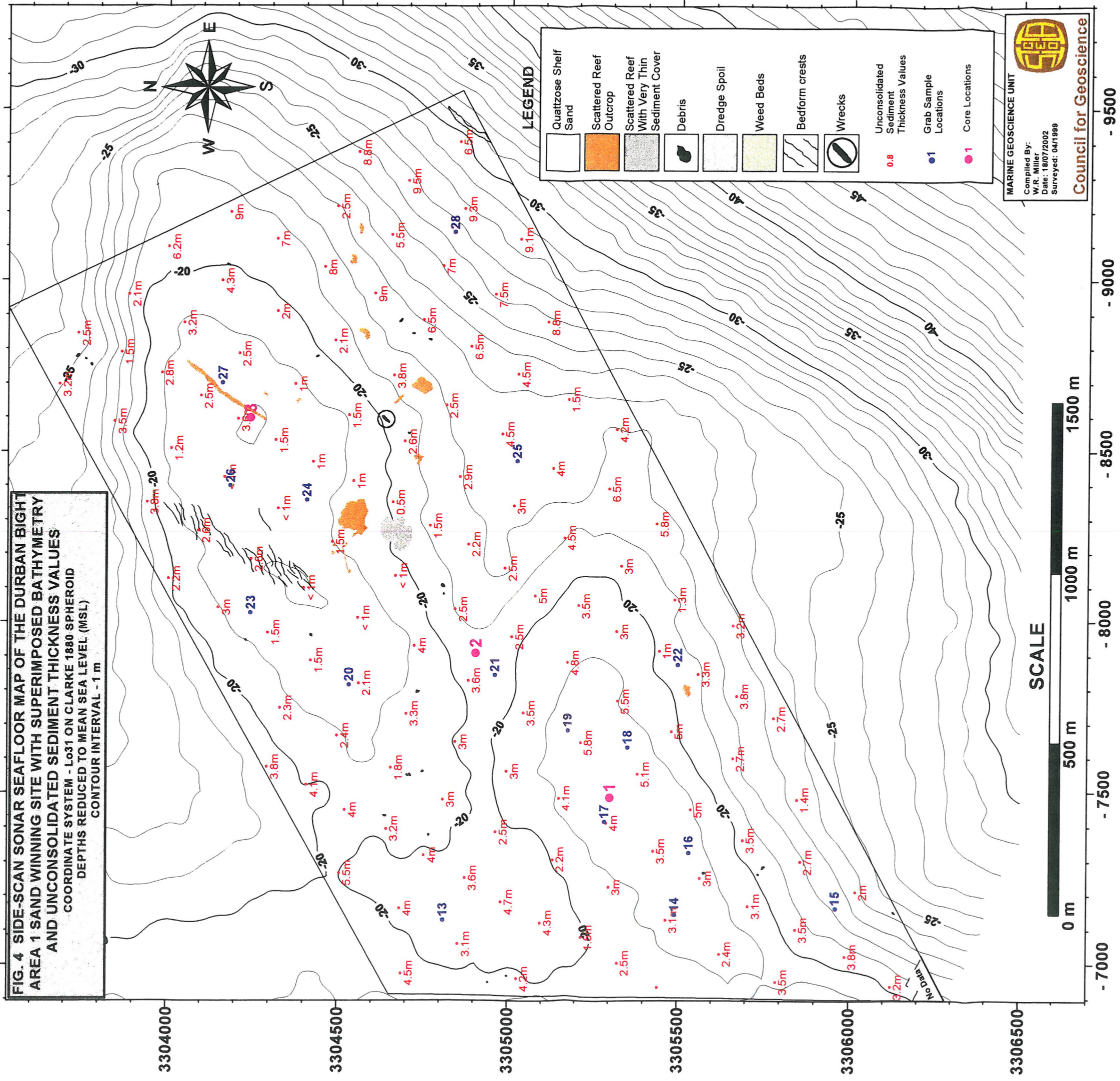


The weak to moderately reflective, even toned planar acoustic facies is by far the most abundant acoustic facies in both of the borrow areas (Figs. 4 & 5). This acoustic facies is typical of fine- to medium - grained unconsolidated shelf sand (i.e. normal near-shore marine sediments). It is evident from studying the side-scan sonar mosaic (Fig. 3) that there are subtle differences between this facies between the two potential borrow areas. The sonographs in Area 2 are uniform and even toned whereas the sonographs from Area 1 show slightly darker patches and are more granular in texture. This is a function of grain-size of the sediments and indicates that the sediments in Area 1 and particularly on the northern sediment mound are coarser grained than the sediments in Area 2. This observation is supported by the analyses conducted on the sediment samples (Sections 8 & 9). The presence of a group of moderately reflective granular lineations at the centre of the northern sand mound in Area 1 indicates the presence of a subaqueous bedform field. The lineations measure between 50 m and 150 m in length and represent subaqueous bedform crests which are oriented roughly northeast - southwest (Fig. 4). The bedforms have a wavelength of $\pm 10 - 20$ m and have an estimated amplitude of ± 0.5 m. These are essentially ephemeral features which are instrumental in transporting sediment southwards under the influence of the Agulhas current.

The areas of scattered reef outcrop are sparse and form a scattered outcrop pattern in the Area 1 borrow site (Fig. 4). The scattered reef exposures are characterised by, isolated, highly reflective, granular to blotchy, sometimes linear sonograph images with or without shadow areas (white) on their leeward side. Small acoustic shadows associated with this acoustic facies suggests that the reef exposures are subdued, with less than 2m of microtopography. The distribution pattern of scattered reef outcrop in Area 1 is haphazard but occurrences are concentrated in a broad band in the central to northeastern part of the Area 1 borrow site (Fig.4). The largest occurrences of scattered reef outcrop measure ± 100 m by 100m, 50 m by 30 m and 300m by 10m. The broad band of scattered reef outcrop in Area 1 is roughly on strike with the shallow pinnacles of No.1 Reef (Figs. 2 & 4). No scattered reef outcrops were identified in the Area 2 borrow site.

An acoustic facies, measuring ± 100 m by 75 m, which is characterised by moderate to high reflectivity and granular to nodular texture to the southwest of the largest exposure of scattered reef in Area 1 is interpreted as reef that is buried beneath a thin sediment veneer.

FIG. 4 SIDE-SCAN SONAR SEAFLOOR MAP OF THE DURBAN BIGHT AREA 1 SAND WINNING SITE WITH SUPERIMPOSED BATHYMETRY AND UNCONSOLIDATED SEDIMENT THICKNESS VALUES
 COORDINATE SYSTEM - LQ31 ON CLARKE 1880 SPHEROID
 DEPTHS REDUCED TO MEAN SEA LEVEL (MSL)
 CONTOUR INTERVAL - 1 m



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SCALE
 0 m 500 m 1000 m 1500 m

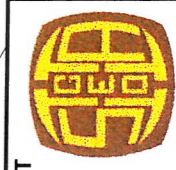
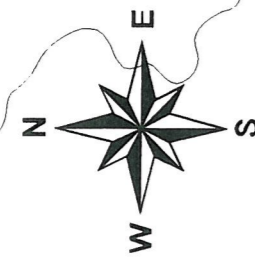
- 7000 - 7500 - 8000 - 8500 - 9000 - 9500

It is very likely that all the reef in Area 1 (exposed /buried) forms a southern extension of the No. 1 Reef complex which is now largely buried. No. 1 Reef is an aeolianite Reef complex which consists of carbonate cemented fine to medium grained sand with a typical uniaxial compressive strength of ± 70 Mpa (pers. comm. Dr. P.J. Ramsay). The reef areas represent ancient linear coastal dune deposits which accumulated during periods of lower sea-level. By virtue of the shell fragment content of the coastal dune sediments, the dune core underwent cementation by a mechanism of dissolution of calcium carbonate on dune crests by rainwater and re-precipitation of the calcium carbonate at depth when the calcium rich pore waters encountered the meteoric interface. A subsequent rise in sea-level has left the now lithified dune sediments (aeolianite) as linear reefs on the seafloor.

Both Area 1 and Area 2 are characterised by a very scattered and random distribution of small highly reflective sonar contacts with little or no acoustic shadow (Figs. 4 & 5). The reflective objects are highly variable in size and shape and none have a characteristic shape that could lead to an unequivocal identification of what these objects represent. The random distribution of these contacts over large areas of unconsolidated shelf sediment precludes the possibility that these contacts represent small reef exposures. The objects in question are probably man-made and their occurrence and distribution are probably related to debris being thrown overboard by passing ship traffic. The objects have a random arrangement but some occur in fairly dense clusters. The debris in Area 1 has a very scattered distribution and the objects are usually less than 10 m in diameter. Area 2 also shows a random and scattered pattern of smaller debris (< 10 m in diameter) but also shows two clusters of larger more elongate debris contacts near the centre of the borrow site (Fig. 5). Individual debris contacts in these clusters reach a maximum of ± 50 m in length. The largest debris contact is located in the northeastern corner of Area 2 and measures 55m by 45 m. This sonar contact is a composite of several small contacts surrounding a larger central object, but has been digitized as a single contact as it is impossible to resolve individual objects.

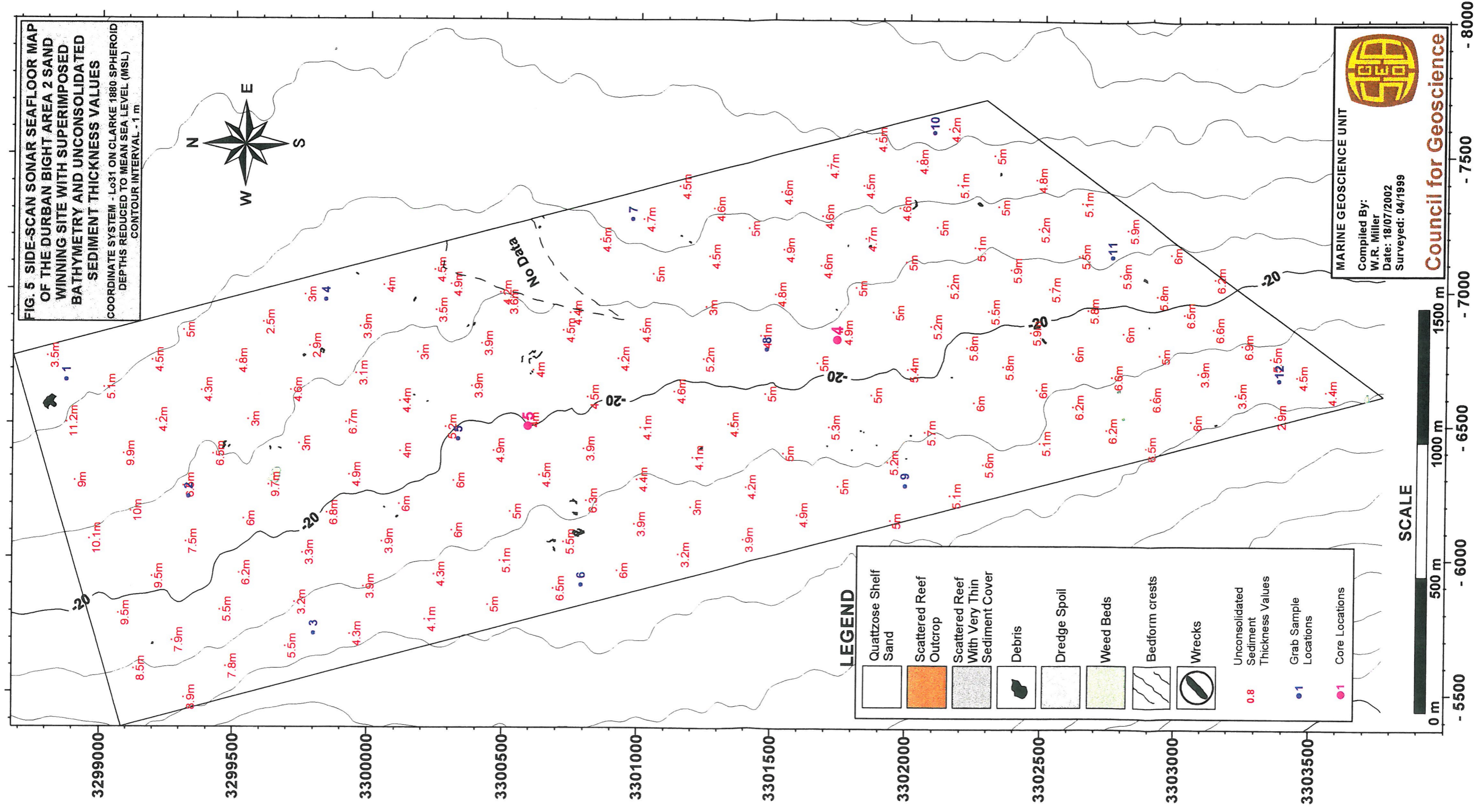
Dredge spoil takes the form of linear, dark patches of moderately reflective sediment of variable size and orientation on the seafloor (Miller, 2000). Only one example of dredge spoil is evident in the southeastern corner of Area 1, adjacent to the modern dump site. The dredge spoil measures ± 165 m in length by 15 m wide. The size of the dredge spoil site and degree of acoustic reflection are probably an indication of how long the dredge spoil has been resting on

FIG. 5 SIDE-SCAN SONAR SEAFLOOR MAP OF THE DURBAN BIGHT AREA 2 SAND WINNING SITE WITH SUPERIMPOSED BATHYMETRY AND UNCONSOLIDATED SEDIMENT THICKNESS VALUES
 COORDINATE SYSTEM - Lo31 ON CLARKE 1880 SPHEROID
 DEPTHS REDUCED TO MEAN SEA LEVEL (MSL)
 CONTOUR INTERVAL - 1 m



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LEGEND

	Quattzose Shelf Sand
	Scattered Reef Outcrop
	Scattered Reef With Very Thin Sediment Cover
	Debris
	Dredge Spoil
	Weed Beds
	Bedform crests
	Wrecks
	Unconsolidated Sediment Thickness Values
	Grab Sample Locations
	Core Locations

SCALE



0 m 500 m 1000 m 1500 m - 5500 - 6000 - 6500 - 7000 - 7500 - 8000

the seafloor i.e. recent deposits of dredge spoil being more compact in size and more reflective in nature (darker) than dredge spoil that has been lying on the seafloor for longer periods of time.

Weed beds take the form of small, spherical to larger more irregularly shaped sonar contacts with no acoustic shadows. These acoustic contacts are highly reflective at the centre and become less reflective towards the margins. The weed beds are all located on the more stable sea-floor conditions of Area 2 and are always characterised by diffuse or “fuzzy” margins on the sonographs. The largest weed bed is located in the central northern part of Area 2 and measures ± 60 m in length by 40 m in width. Several smaller examples are located in the southwestern part of Area 2.

Only one wreck is evident in the survey areas and is located in the central-eastern part of Area 1 (Fig. 4). The wreck measures 30 m in length by 7.5 m in width and stands ± 1.5 m off the sea-floor. The high acoustic reflectivity and intact nature of the wreck image suggest that it is a steel hull vessel.

The primary objective of this report is to identify areas that are most suitable for sand winning and to delineate problem areas where dredging activity might be ill advised. Such problem areas in the context of the identified acoustic facies are; exposed reef areas, areas of reef that are covered with a thin sediment veneer, wreck sites and sites of debris accumulation. The dredge spoil located in the southeastern corner of Area 1 should also be avoided as this represents an area of the seafloor which has elevated mud concentrations in the sediments (Miller *et al*, 2001). Areas delineated with the above mentioned acoustic facies on the seafloor maps (Figs. 4 & 5) should not be considered as areas suitable for sand winning.

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7. UNCONSOLIDATED SEDIMENT THICKNESS

Unconsolidated sediment thickness values are illustrated as point data on the side-scan sonar seafloor maps (Figs. 4 & 5). Unconsolidated sediment thickness values range from 0 m in Area 1 to as much as 11.2 m in the northern part of Area 2. Sediment thickness values are at a minimum in the vicinity of reef or scattered reef outcrop and in areas where the aeolianite reef is continuous beneath the sediment.

Unconsolidated sediment thickness values in Area 1 vary from 0 m in areas of reef outcrop to as much as 9.5 m, with an average thickness of 3.6 m. The thickest accumulations of unconsolidated sediment occur in the southeastern corner of Area 1 where sediments attain a thickness of between 5.5m and 9.5 m (Fig. 4). Consistently thick accumulations of unconsolidated sediment occur in the western extremity of Area 1 where sediment accumulations of between 1.4 m and 5.8 m are evident. The sediment thins markedly in the central part of the borrow site, particularly in the vicinity of the reef outcrops (Fig. 4). Sediment thickness values range from 0 m to 4.5 m in this area and northern part of this borrow site. The average sediment thickness in Area 1 is ± 3.6 m.

Unconsolidated sediment accumulations in Area 2 vary from a minimum of 2.5 m to a maximum of 11.2 m, with a mean value of 5.2 m. The thickest sediment accumulations occur in the northern part of Area 2 adjacent to the Mgeni estuary. Unconsolidated sediment accumulation ranges from 2.9 m to 6.9 m in the southern part of Area 2 with the thickest accumulations occurring in water deeper than 19 m. The central and northern central part of Area 2 is characterised by variable unconsolidated sediment accumulations and average sediment thickness in this area averages ± 4.5 m. There is no reef exposure in Area 2 and in general there is a significant thickness of unconsolidated sediment throughout this borrow site.

8. GRAB SAMPLES

Twenty eight grab samples were collected to investigate the sedimentary character of the shelf sand in the proposed sand winning areas. Twelve samples were collected in Area 2 and sixteen were collected in Area 1 (Figs. 4 & 5). A full set of laboratory analyses including; sample position, gravel %, mud %, median, mean, sorting, skewness, dry density and carbonate % are presented in Appendix 1. Cumulative frequency curves and photographs of representative sediment samples are presented in Appendices 2 & 3. **Note:** Sediment sorting is reported in terms of geological principles, whereby a well sorted sand has a very narrow grain-size distribution and a poorly sorted sand has a broader grain-size distribution.

8.1 Sediment Description - Area 1

The grab samples in Area 1 were collected in water depths ranging from 18 m to 27 m (Fig. 4). The grab samples from Area 1 are characterised by light olive to light reddish brown, moderately well sorted to very well sorted, subangular to well rounded, medium-grained, clean free flowing sands with high calcium carbonate contents, low gravel contents and low interstitial mud (< 63 µm) contents. The sediments have an average “loose” dry density of 1.572 T/m³ and an average “compact” (50 blows of compaction) dry density of 1.622 T/m³. The sedimentary characteristics of the Area 1 grab samples are summarised in the Table 8.1 below.

<i>n</i> = 16	Median mm	Mean mm	Sorting	Gravel %	Mud %	Dry Density	CaCO ₃ %
Min.	0.213	0.227	0.25	0	0.97	1.525 T/m ³	8.85
Max.	0.444	0.474	0.62	1.35	1.75	1.689 T/m ³	23.47
Ave.	0.304	0.322	0.45	0.49	1.34	1.622 T/m ³	12.77
Color	Light olive - light reddish brown						
Sediment Type	Well sorted medium-grained sand						
Sediment Maturity	Subangular to rounded						

Table 8.1 Sedimentary characteristics of Area 1 grab samples.

8.2 Sediment Description - Area 2

The grab samples in Area 2 were collected in water depths ranging from -18 m to -23 m (Fig. 5). The grab samples from Area 2 are characterised by dark reddish brown to light grey, well sorted to very well sorted, subangular to rounded, fine-grained, clean free flowing sands with high calcium carbonate contents, low gravel contents and low interstitial mud contents. The sediments have an average “loose” dry density of 1.468 T/m³ and an average “compact” dry density of 1.536 T/m³. The sedimentary characteristics of the Area 2 grab samples are summarised in Table 8.2 below.

<i>n</i> = 12	Median mm	Mean mm	Sorting	Gravel %	Mud %	Dry Density	CaCO ₃ %
Min.	0.123	0.122	0.29	0	1.44	1.502 T/m ³	3.19
Max.	0.203	0.217	0.45	0.34	2.62	1.610 T/m ³	23.47
Ave.	0.147	0.149	0.34	0.04	2.04	1.535 T/m ³	15.93
Color	Dark reddish brown - light grey						
Sediment Type	Very well sorted fine-grained sand						
Sediment Maturity	Subangular to rounded						

Table 8.2 Sedimentary characteristics of Area 2 grab samples.

8.3 Summary

On average the gravel, mud and calcium carbonate contents of the grab samples from the two borrow sites are fairly similar. The Area 1 grab samples are however, coarser-grained, less well sorted and have higher dry densities than the Area 2 sediments.

9. CORE SAMPLES

A total of five sediment cores measuring between 4.29 m and 4.57 m were collected in the proposed borrow sites, Cores 1, 2 & 3 from Area 1 and Cores 4 & 5 from Area 2. Laboratory analyses, cumulative frequency curves and representative sediment photographs are presented in Appendices, 1, 2 & 3. Core logs with laboratory analyses are presented below.

9.1 Core 1

Core 1 consists of light olive to dark reddish brown, moderately well sorted to very well sorted, subangular to rounded, fine-to medium-grained, clean free flowing sands with high calcium carbonate content, and low interstitial mud (< 63 μm) and gravel contents. The sediments have an average “loose” dry density of 1.490 T/m³ and an average “compact” (50 blows of compaction) dry density of 1.543 T/m³. The sedimentary succession of Core 1 consists of numerous upward fining sedimentary units, which are interbedded with more homogenous sedimentary units. The sediments are rich in shell fragments and contain occasional subangular to well rounded pebbles which are normally concentrated at the base of the upward fining units. Individual sedimentary units vary between 0.4 m to 1.0 m in thickness and are probably related to ancient dumping activity. The sedimentary characteristics of Core 1 samples are illustrated in Figure 6 and summarised in Table 9.1 below.

<i>n</i> = 13	Median mm	Mean mm	Sorting	Gravel %	Mud %	Dry Density	CaCO₃ %
Min.	0.186	0.191	0.35	0	0.58	1.464 T/m ³	14.04
Max.	0.25	0.269	0.65	8.63	2.84	1.631 T/m ³	29.61
Ave.	0.216	0.23	0.49	0.81	1.67	1.543 T/m ³	19.48
Color	Light olive - dark reddish brown						
Sediment Type	Well sorted fine- to medium-grained sand						
Sediment Maturity	Subangular to rounded						

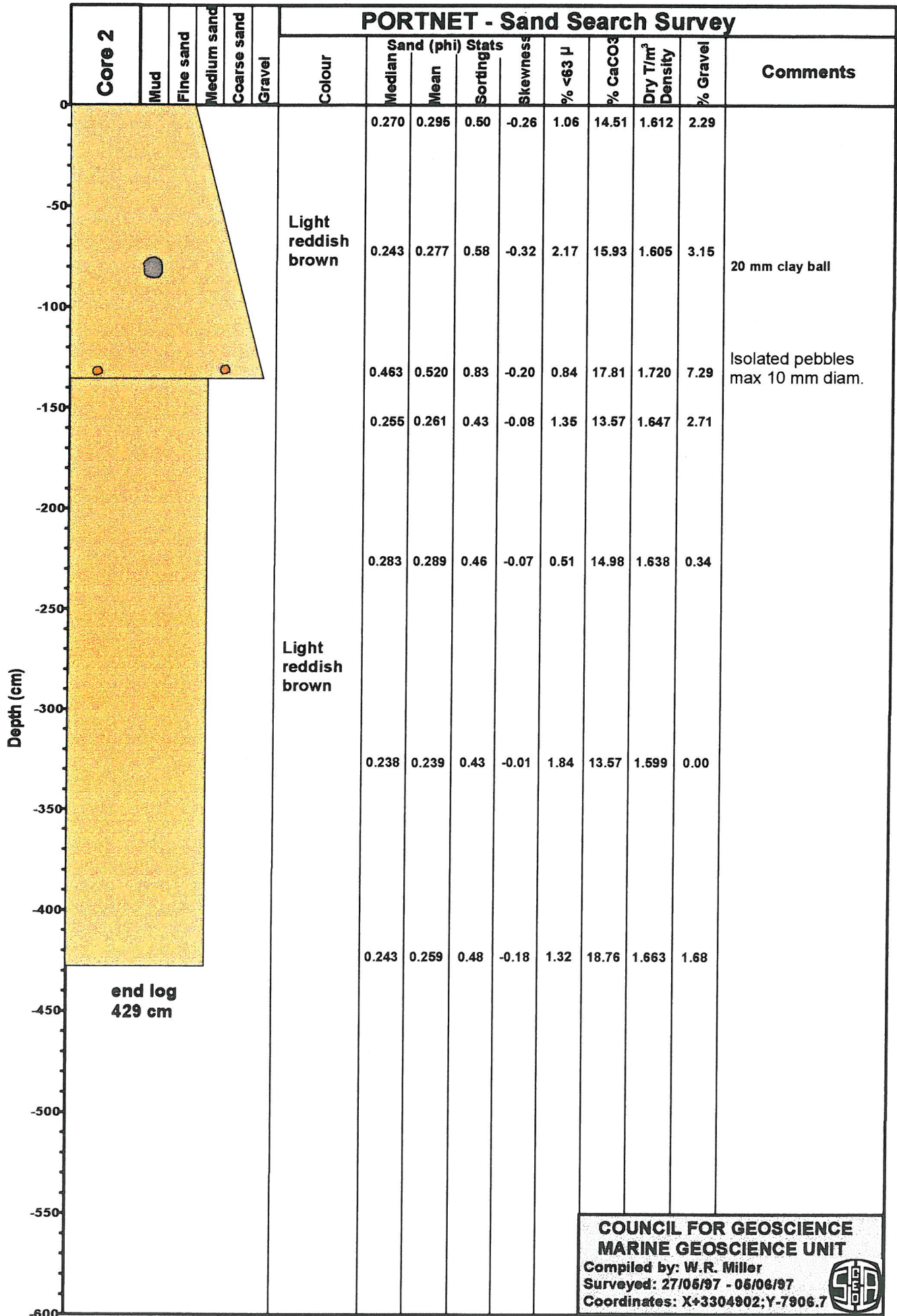
Table 9.1 Sedimentary characteristics of Core 1 sediment samples.

9.2 Core 2

Core 2 consists of light reddish brown, moderately well sorted to well sorted, subangular to rounded, medium-grained, clean free flowing sands with high calcium carbonate content and low interstitial mud (< 63 µm) contents. The sediments have an average “loose” dry density of 1.584 T/m³ and an average “compact” dry density of 1.641 T/m³. The sedimentary succession of Core 1 consists of an upper unit of upward fining sand, rich in shell fragments with a gravel base containing sub angular to rounded pebbles of up to 20 mm in diameter. The upper unit measures 1.35 m in thickness and overlies a more homogenous basal unit consisting of massive, medium grained, shell rich sand with occasional subangular to well rounded pebbles. The upward fining nature of the upper unit is probably related to historical dumping activity and later reworking by normal marine processes. The sedimentary characteristics of Core 2 are illustrated in Figure 7 and summarised in Table 9.2 below.

<i>n</i> =7	Median mm	Mean mm	Sorting	Gravel %	Mud %	Dry Density	CaCO₃ %
Min.	0.238	0.239	0.43	0	0.51	1.599 T/m ³	13.57
Max.	0.463	0.52	0.83	7.29	2.17	1.720 T/m ³	18.76
Ave.	0.285	0.306	0.53	2.49	1.3	1.641 T/m ³	15.59
Color	Light reddish brown						
Sediment Type	Moderately well sorted medium-grained sand						
Sediment Maturity	Subangular to rounded						

Table 9.2 Sedimentary characteristics of Core 2 sediment samples.



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Fig. 7 Core 2

9.3 Core 3

Core 3 consists of light reddish brown to dark yellow, moderately sorted to well sorted, subangular to rounded, medium-grained, free flowing sands with high calcium carbonate contents and low interstitial mud contents. The core consists of an upper, upward fining unit which is 0.9 m thick and has a well defined gravel base. This unit overlies three homogenous sedimentary units which range in thickness from 0.1 m - 0.35 m. The basal part of the sedimentary succession comprises an upward fining sedimentary unit which has a minimum thickness of 2.65 m. The gravel content of this core is fairly high and is concentrated at the base of the upper upward fining unit and in the sedimentary units which have a dark yellow colouration. The basal unit has very low gravel contents and is believed to represent normal marine sedimentation while the upper unit is probably related to dumping activity. Exposed reef was sited adjacent to this core site by the commercial diver in attendance during the coring procedure. Core refusal was encountered at a depth of 4.30 m probably due to the core barrel striking the buried reef surface. The elevated gravel content of this core is probably related to the higher concentration of bioclastic gravel in close proximity to the reef (Fig. 4). The sedimentary character of Core 3 is illustrated in Figure 8 and summarised in Table 9.3 below.

<i>n</i> = 10	Median mm	Mean mm	Sorting	Gravel %	Mud %	Dry Density	CaCO ₃ %
Min.	0.213	0.211	0.35	0	0.27	1.554 T/m ³	9.32
Max.	0.387	0.432	0.77	34.54	4.85	1.779 T/m ³	32.91
Ave.	0.289	0.314	0.52	8.4	1.83	1.651 T/m ³	16.68
Color	Light reddish brown to dark yellow						
Sediment Type	Moderately well sorted medium-grained sand with subordinate gravel lenses						
Sediment Maturity	Subangular to rounded						

Table 9.3 Sedimentary characteristics of Core 3 sediment samples.

9.4 Core 4

Core 4 consists of dark reddish brown to light grey, well sorted to very well sorted, subangular to rounded, fine-grained, free flowing sands with high calcium carbonate contents and moderate to low interstitial mud contents. Gravel content of the sediments is typically low with the only exception being a shelly gravel lag which is evident at a core depth of -0.7 m to -0.8 m. The sediments have an average “loose” dry density of 1.411 T/m³ and an average “compact” dry density of 1.475 T/m³. The sedimentary succession is divided into a thin (0.57 m), dark reddish brown to light grey upper unit and a thick (3.58 m), light grey basal unit which are separated by the moderately well developed shelly gravel lag deposit (Fig.9). The sedimentary nature of Core 4 is illustrated in Figure 9 and summarised in Table 9.4 below.

<i>n</i> = 7	Median mm	Mean mm	Sorting	Gravel %	Mud %	Dry Density	CaCO ₃ %
Min.	0.131	0.131	0.21	0	2.2	1.391 T/m ³	22.53
Max.	0.15	0.172	0.43	8.35	3.57	1.628 T/m ³	32.44
Ave.	0.142	0.149	0.31	1.56	2.91	1.475 T/m ³	26.71
Color	Dark reddish brown to light grey						
Sediment Type	Well sorted to very well sorted fine-grained sand with subordinate shelly gravel lags						
Sediment Maturity	Subangular to rounded						

Table 9.4 Sedimentary characteristics of Core 4 sediment samples.

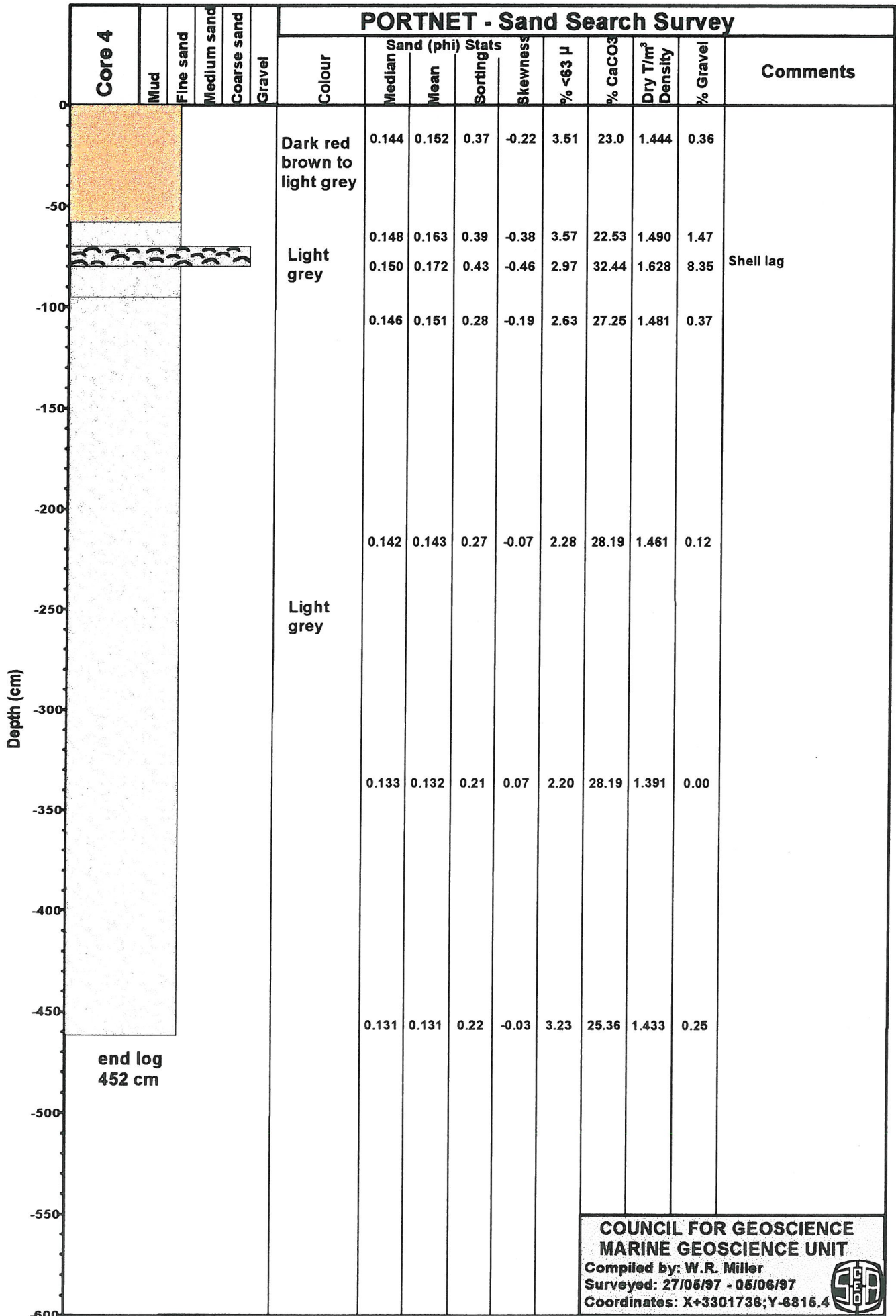


Fig. 9 Core 4.

9.5 Core 5

Core 5 consists of dark reddish brown to light grey, moderately well sorted to well sorted, fine-grained sand with high calcium carbonate contents and moderate to low interstitial mud contents. The sediments have an average “loose” dry density of 1.460 T/m³ and an average “compact” dry density of 1.526 T/m³. Gravel content of the sediments is typically low except at the base of the core where gravel concentrations of 8 % - 14 % are encountered (Fig. 10). The sedimentary succession consists of a 1.15 m thick upper unit which is characterised by a dark reddish brown to light grey colour and a lower, light grey unit which measures 3.23 m in thickness. The sedimentary units are very similar in sedimentary character except for the base of the lower unit where there is an increase in the mean grain-size, gravel content and dry density. The base of Core 5 is characterised by a light olive gravel rich horizon which is believed to be the top of a much older sedimentary unit identified from the sub-bottom profiling records. The sedimentary nature of Core 5 is illustrated in Figure 10 and summarised in Table 9.5 below.

<i>n</i> = 9	Median mm	Mean mm	Sorting	Gravel %	Mud %	Dry Density	CaCO ₃ %
Min.	0.13	0.13	0.22	0	0.73	1.382 T/m ³	17.34
Max.	0.401	0.438	0.88	14.04	2.99	1.818 T/m ³	34.32
Ave.	0.173	0.19	0.46	3.44	2.15	1.526 T/m ³	24.57
Color	Dark reddish brown to light grey						
Sediment Type	Moderately well sorted to well sorted, fine-grained sand with subordinate gravel lenses						
Sediment Maturity	Subangular to rounded						

Table 9.5 Sedimentary characteristics of Core 5 sediment samples.

9.6 Summary

The Area 1 cores show more textural variation with depth than the Area 2 cores and on average the Area 1 sediments are coarser grained, show poorer sorting, have lower interstitial mud contents, higher dry densities and lower calcium carbonate contents than the Area 2 sediments.

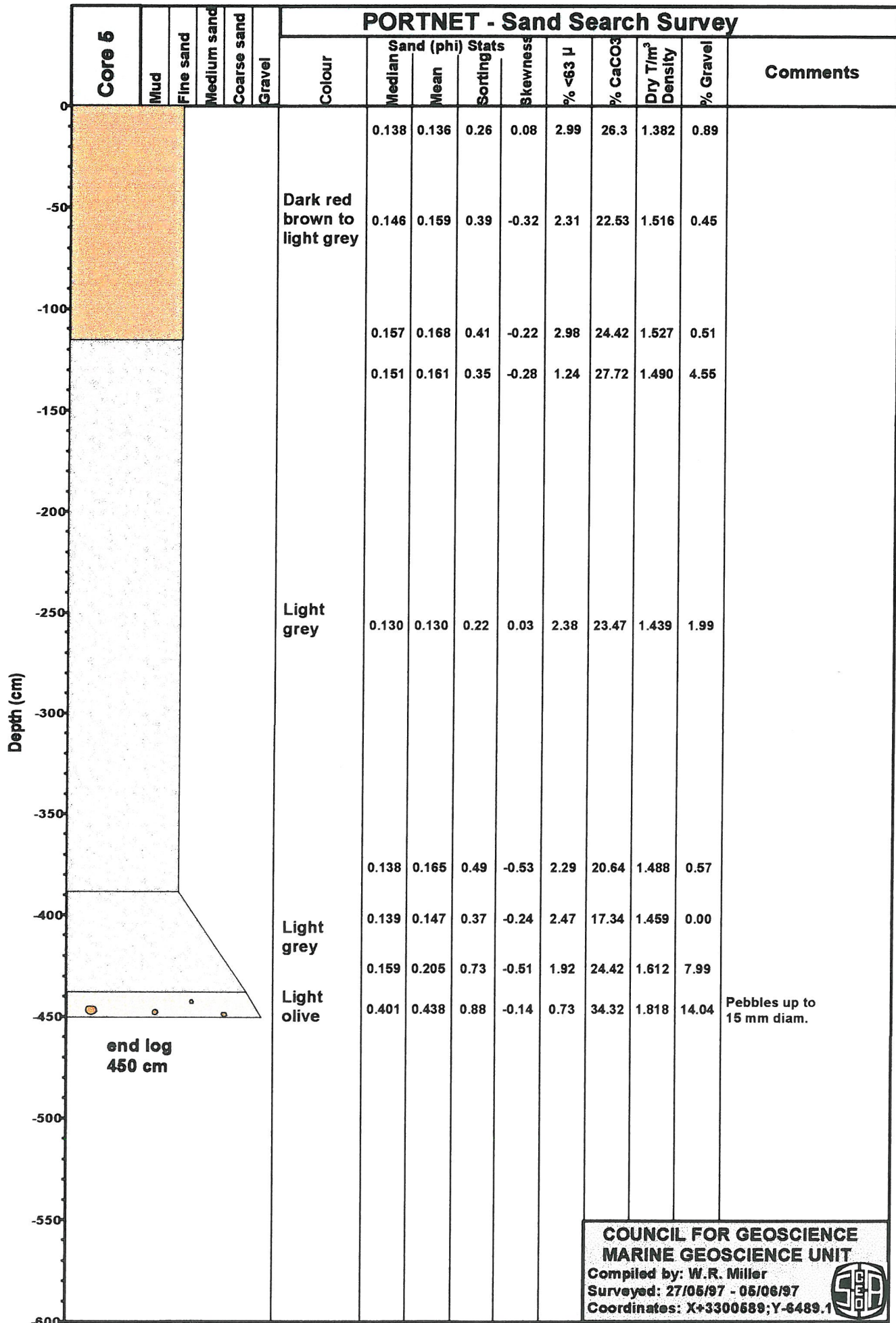


Fig. 10 Core 5

10. DISCUSSION

In terms of weighing up the potential sand winning areas up against each other, there are several factors which must be considered in determining which of the areas will ultimately be favoured. Important criterion include; the nature of the sediments to be dredged, water depth, proximity to "hard" substrates, availability of sufficient sediment volumes, predictability of dredge conditions with increased sediment depth, proximity to the area where the sediments will be used and the potential environmental consequences of dredging.

The geophysical data from the Council for Geoscience's data base were used to assess water depth, unconsolidated sediment thickness and seafloor conditions in each of the potential borrow areas and to highlight the presence of any "hard" objects or substrates that could be detrimental to dredging activity. The bathymetry data shows similar water depths in both survey blocks with depths ranging from -19 m to -32 m in Area 1 and depths ranging from -18 m to -23 m in Area 2. Both potential sand winning areas have large areas of sediment cover on gently sloping seafloor in shallow water and therefore the bathymetric data neither favours nor rejects either of the borrow sites.

Of the seven acoustic facies identified from the side-scan sonar data, only four can be viewed as potential hazards for dredging activity. The most significant of these are the areas of scattered reef exposure and areas where reef is buried beneath a thin veneer of sediment. These substrates are confined to the Area 1 survey block, in particular the northeastern section (Fig. 4). The reef exposures are probably aeolianite which characteristically have unconfined uniaxial compressive strengths in the order of 70 Mpa. These "hard" substrates should be avoided by dredging activity. The smaller sonar contacts which comprise, debris occurrences and ship wrecks also represent "hard" (probably metal) objects resting on the seafloor and present obvious problems for sediment dredging. These objects should also be avoided during sand dredging activity. The side-scan sonar data interpretation would seem to favour Area 2 as the better sand winning site as there are no reef occurrences in that survey block.

The unconsolidated sediment thickness in the proposed sand winning areas was measured from sub-bottom profiling records and represents the minimum thickness of sediment that can be removed by dredging. Unconsolidated sediment thickness varies from 0 m in areas of reef outcrop to as much as 9.5 m in Area 1 and averages 3.6 m. The presence of the shallow No. 1 reef pinnacles to the northeast and the presence of reef exposure within the Area 1 borrow site, is cause for concern as it implies that the reef complex is continuous beneath the Area 1 sediments. The line spacing of 150 m which was used during the collection of the geophysical data, precludes the possibility of knowing the location of all buried reef pinnacles, but is still adequate enough to highlight safe dredging areas. These areas are represented by the thick sediment accumulations in the southeastern corner of the Area 1 borrow site and the area adjacent to its western boundary (Fig. 4). Unconsolidated sediment thickness in Area 2 varies from a minimum of 2.5 m to a maximum of 11.2 m and averages 5.2 m. Area 2 is characterised by regionally developed thick sediment accumulations and inadequate sediment thickness is not perceived to be a problem in this borrow site.

Probably the most important criterion to be considered when weighing up the two potential sand winning areas, is the nature of the sediments. The sediments are, after all, to be dredged for a specific purpose (backfill in this case). The emphasis of this report has therefore been to describe the sediments from each borrow site in great detail and to arrive at a set of sedimentary parameters which best describes the sediments.

A total of 74 sediment samples were taken as grab samples or as sub-samples from sediment cores, 46 from Area 1 and 28 from Area 2. The samples were subjected to a suite of laboratory tests and numerous sedimentary parameters including, median grain-size, mean grain-size, sediment sorting, sediment skewness, mud content, gravel content, calcium carbonate content and dry density were measured. Representative values for each of the sedimentary parameters for each survey area were calculated by averaging all the sedimentary analyses for each group of samples i.e. grab samples and core samples. Tables 10.1 and 10.2 compare the representative sedimentary parameters calculated from the grab samples and core samples from each of the borrow sites, and then combines all laboratory analyses to produce a final set of analyses, which is believed to be representative of the sedimentary succession for each of the

potential sand winning areas.

	Median mm	Mean mm	Sorting	Gravel %	Mud %	Dry Density	CaCO ₃ %
Grabs (<i>n</i> = 16)	0.304	0.322	0.45	0.49	1.34	1.622 T/m ³	12.77
Cores (<i>n</i> = 30)	0.256	0.276	0.51	3.73	1.64	1.602 T/m ³	17.64
All (<i>n</i> = 46)	0.273	0.292	0.49	2.6	1.54	1.609 T/m³	15.95

Table 10.1 Representative sediment characteristics of Area 1 sediment samples.

	Median mm	Mean mm	Sorting	Gravel %	Mud %	Dry Density	CaCO ₃ %
Grabs (<i>n</i> = 12)	0.147	0.149	0.34	0.04	2.04	1.535 T/m ³	12.77
Cores (<i>n</i> = 16)	0.16	0.172	0.39	2.62	2.48	1.504 T/m ³	25.51
All (<i>n</i> = 28)	0.154	0.162	0.37	1.51	2.29	1.517 T/m³	21.4

Table 10.2 Representative sediment characteristics of Area 2 sediment samples.

Tables 10.1 and 10.2 show that Area 1 sediments are in general coarser grained and less well sorted than Area 2 sediments. Area 1 sediments have on average marginally higher gravel contents and marginally lower interstitial mud contents than Area 2 sediments, but have significantly lower calcium carbonate contents and significantly higher “compact” dry densities than the Area 2 sediments. In terms of sediment predictability, Area 2 sediments are more homogenous than Area 1 sediments, the latter shows significant variation in texture with depth.

The coarser grain-size, poorer sorting, lower interstitial mud content and higher dry densities of the Area 1 sediments probably makes these sediments more suitable for use as backfill than the Area 2 sediments. In terms of environmental considerations the Area 1 sediments are also favored, as large volumes of these sediments represent artificially dumped material. Dredging of this material is considered favourable to disturbing the more pristine seafloor underlain by Area 2 sediments.

*Area 1
Area 2*

11. RECOMMENDATIONS

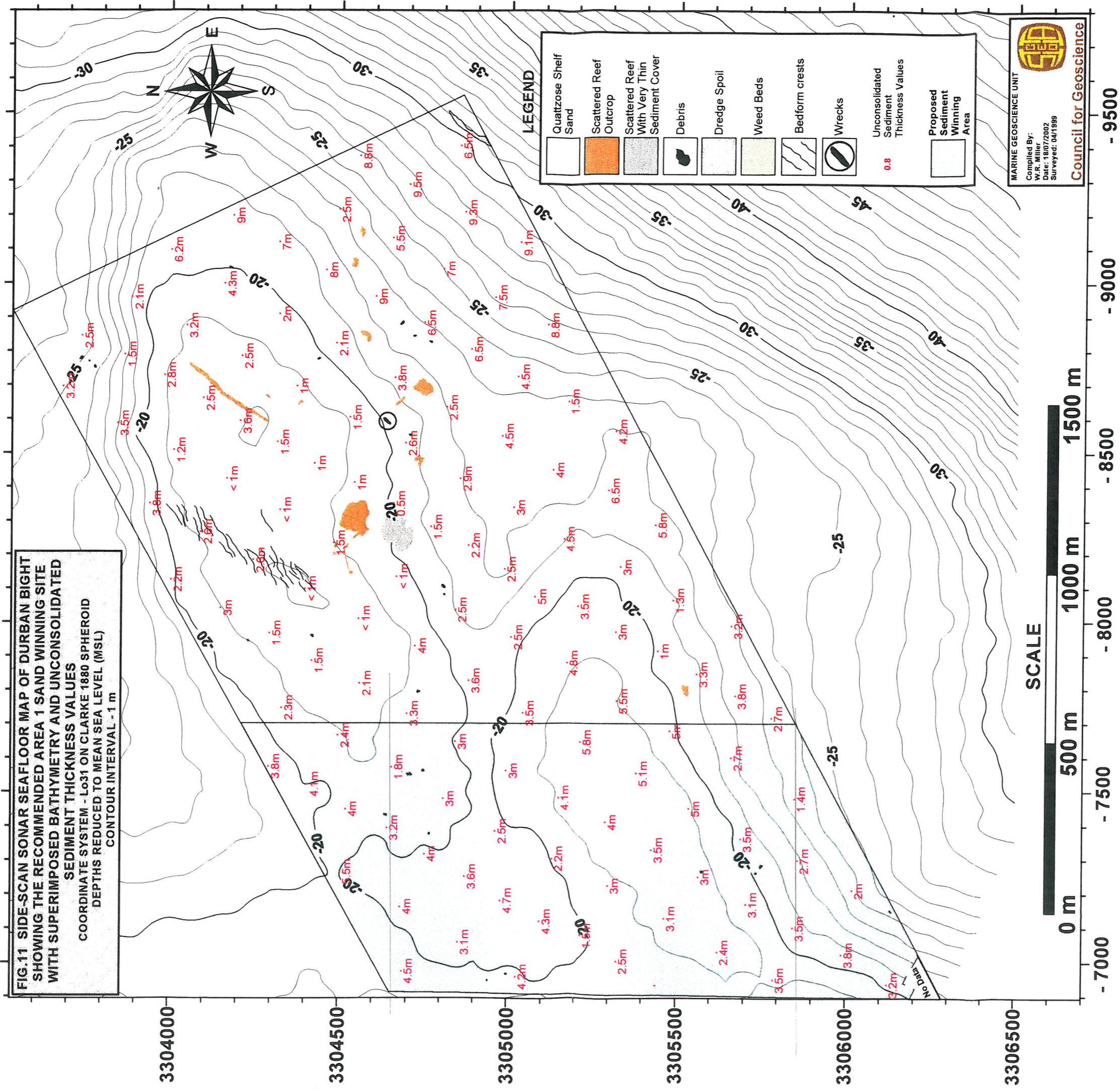
Based on all the above arguments, the most promising sand winning sites (in the author's opinion) have been selected from each of the borrow sites and are illustrated in Figures 11 & 12. The most favourable area for sand winning in Area 1 is a $\pm 800\text{m}$ wide corridor of adjacent to the western boundary of the survey area (Fig. 11). The lack of reef exposure, close proximity to the harbour entrance, the sparse nature of debris accumulations and availability of adequate sediment thickness (3 - 4 m) are criterion which support this statement.

The lack of reef exposure, sparse distribution of debris and almost regional availability of thick unconsolidated sediment deposits in Area 2, makes the borrow site suitable for sand winning. In light of economic considerations, the southern part of Area 2 (Fig. 12), is by virtue of the closer proximity to the harbour entrance considered the most favourable area for sand winning in the Area 2 borrow site.

Ultimately the engineering properties of the sediments will determine which of the borrow sites is actually used. Determination of which sediments are more attractive in terms of engineering principles, is however beyond the scope of this report. This report highlights potential sand winning areas from each of the larger borrow sites, which are deemed as the most desirable for sediment dredging. These smaller areas are, however, not entirely free of potentially hazardous dredge conditions due to the random and scattered nature of debris. All areas of debris accumulation within the proposed sand winning areas (Figs. 11 & 12) should be avoided, as these are probably metal objects capable of damaging dredging equipment.

Dredging sediment from both areas and mixing them prior to emplacement may improve the sedimentary character of the backfill material. As a rough guideline a sample of Area 1 sediments (G21) was mixed with Area 2 sediments (G8) in varying proportions and the dry density of this sediment was recalculated to assess the effect of sediment mixing. An optimum mixing proportion of 30 % Area 2 sediments and 70 % Area 1 sediments brought about an increase in "compact" dry density from 1.6097 T/m^3 to 1.6495 T/m^3 of 2.47 % which represents an increase $\pm 2.5 \%$.

**FIG.11 SIDE-SCAN SONAR SEAFLOOR MAP OF DURBAN BIGHT
SHOWING THE RECOMMENDED AREA 1 SAND WINNING SITE
WITH SUPERIMPOSED BATHYMETRY AND UNCONSOLIDATED
SEDIMENT THICKNESS VALUES**
COORDINATE SYSTEM - LO31 ON CLARKE 1880 SPHEROID
DEPTHS REDUCED TO MEAN SEA LEVEL (MSL)
CONTOUR INTERVAL - 1 m



LEGEND

	Quattzose Shelf Sand
	Scattered Reef Outcrop
	Scattered Reef With Very Thin Sediment Cover
	Debris
	Dredge Spoil
	Weed Beds
	Bedform crests
	Wrecks
0.8	Unconsolidated Sediment Thickness Values
	Proposed Sediment Winning Area

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 Compiled By:
 W.K. Miller
 Date: 18/07/2002
 Surveyed: 04/1999



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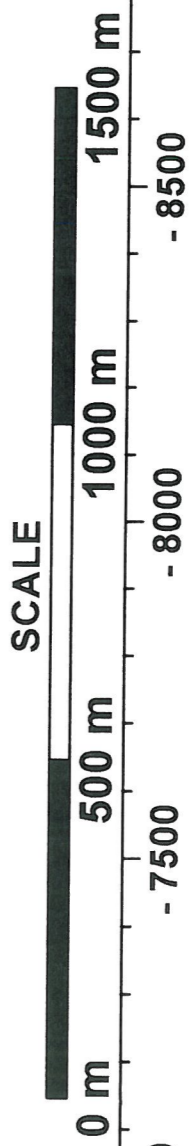


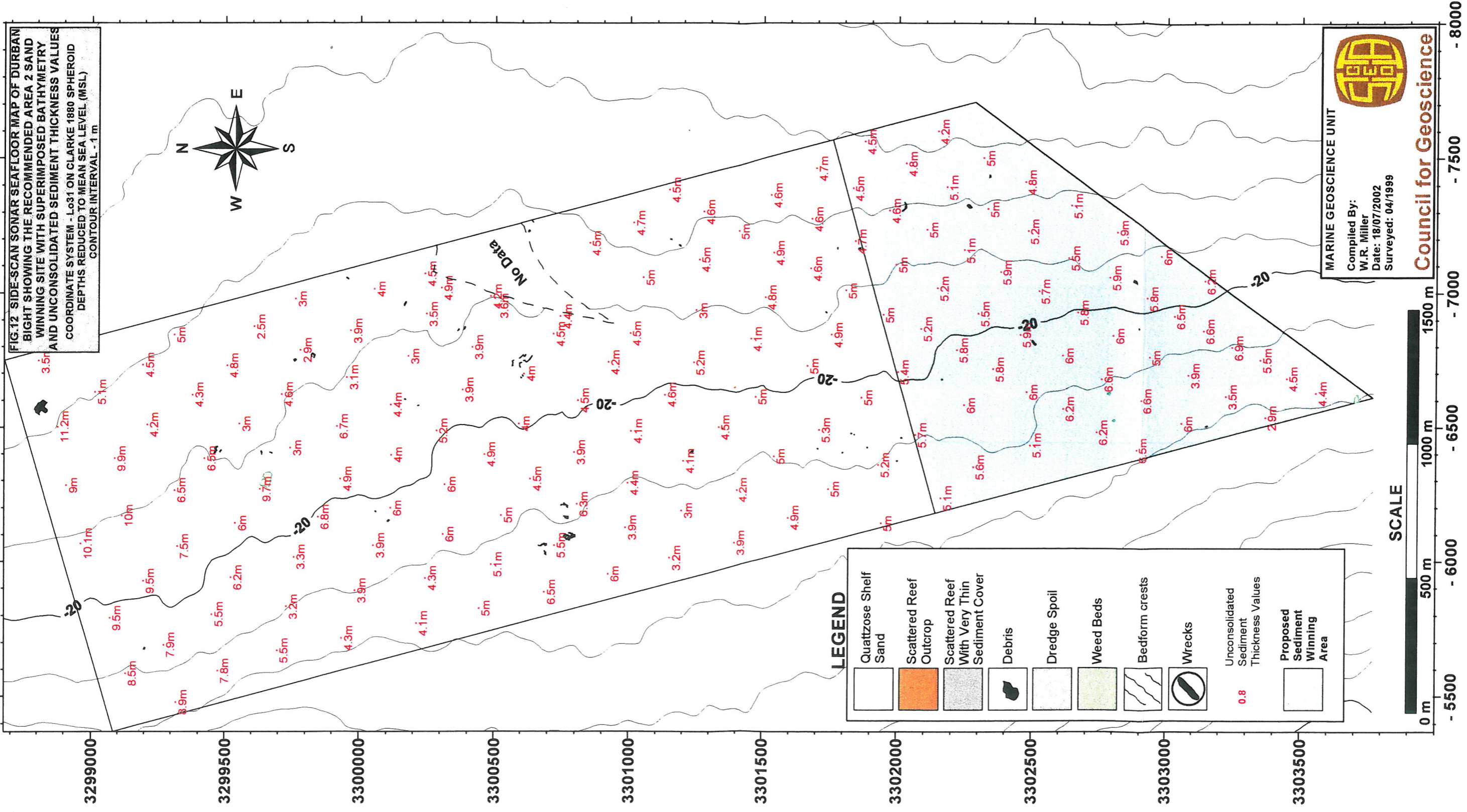
FIG.12 SIDE-SCAN SONAR SEAFLOOR MAP OF DURBAN BIGHT SHOWING THE RECOMMENDED AREA 2 SAND WINNING SITE WITH SUPERIMPOSED BATHYMETRY AND UNCONSOLIDATED SEDIMENT THICKNESS VALUES
 COORDINATE SYSTEM - L031 ON CLARKE 1880 SPHEROID
 DEPTHS REDUCED TO MEAN SEA LEVEL (MSL)
 CONTOUR INTERVAL - 1 m













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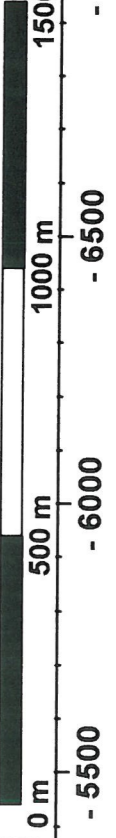
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LEGEND

-  Quattzose Shelf Sand
-  Scattered Reef Outcrop
-  Scattered Reef With Very Thin Sediment Cover
-  Debris
-  Dredge Spoil
-  Weed Beds
-  Bedform crests
-  Wrecks
-  Unconsolidated Sediment Thickness Values
-  Proposed Sediment Winning Area

SCALE



- 5500 - 6000 - 6500 - 7000 - 7500 - 8000

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APPENDIX 1.

SEDIMENTARY LABORATORY ANALYSES

Sample No.	Lo 31 Coordinates		Gravel% (>2000µ)	Mud% (<63µ)	Graphics Statistics from Sand Fraction			Dry Density (Tons/m3)	Carbonate %		
	X	Y			Mean	mm-Mn	mm-Med			Sorting	Skewness
G1	3298870.9	-6656.77	0	1.87	2.85	0.139	0.137	0.29	-0.07	1.515	23.47
G2	3299329.3	-6222.43	0.34	2.39	2.86	0.138	0.137	0.3	-0.04	1.52	21.59
G3	3299799.2	-5715.7	0	1.88	2.66	0.158	0.159	0.39	0.02	1.512	3.19
G4	3299836.1	-6957.76	0	2.26	2.81	0.146	0.143	0.32	-0.11	1.518	21.11
G5	3300330.1	-6439.6	0	2.17	2.94	0.129	0.130	0.31	0.05	1.529	12.62
G6	3300788.6	-5897.31	0.16	2.62	3.03	0.122	0.123	0.38	0.04	1.502	8.38
G7	3300968.9	-7260.02	0	1.85	2.77	0.146	0.143	0.34	-0.12	1.531	19.23
G8	3301475.6	-6777.42	0	1.84	2.77	0.144	0.147	0.34	0.08	1.555	15.93
G9	3301993.8	-6270.69	0	1.85	2.83	0.139	0.141	0.32	0.05	1.567	14.51
G10	3302090.3	-7585.14	0	2.29	2.77	0.146	0.147	0.32	0.02	1.527	16.4
G11	3302753.3	-7126.67	0	1.98	2.59	0.166	0.158	0.35	-0.2	1.54	17.34
G12	3303380.6	-6668.2	0	1.44	2.2	0.217	0.203	0.45	-0.22	1.61	17.34
G13	3304809.4	-7126.67	0	1.64	2.03	0.248	0.245	0.44	-0.04	1.602	13.1
G14	3305490.1	-7144.45	1.15	1.07	1.51	0.35	0.330	0.44	-0.21	1.675	12.62
G15	3305960	-7162.23	1.04	1.57	2	0.271	0.250	0.61	-0.18	1.559	23.47
G16	3305532	-7324.79	0	1.75	1.9	0.268	0.262	0.36	-0.08	1.592	12.62
G17	3305285.6	-7414.96	0.56	1.09	1.5	0.355	0.330	0.47	-0.21	1.629	12.15
G18	3305351.7	-7632.13	0.35	1.27	1.08	0.474	0.444	0.62	-0.15	1.671	10.27
G19	3305176.4	-7680.39	0.13	1.43	1.61	0.327	0.316	0.4	-0.13	1.621	11.21
G20	3304531.3	-7813.74	0.66	1.34	1.28	0.412	0.382	0.52	-0.22	1.644	13.57
G21	3304959.3	-7842.95	0	1.52	1.62	0.326	0.306	0.44	-0.2	1.61	12.15
G22	3305496.5	-7873.43	0.47	1.21	1.27	0.416	0.374	0.59	-0.26	1.658	11.21
G23	3304243	-8024.56	0.17	1.15	1.7	0.308	0.289	0.39	-0.23	1.663	11.21
G24	3304405.5	-8356.03	1.35	1.27	1.73	0.302	0.283	0.39	-0.23	1.656	12.15
G25	3305020.2	-8470.33	0	1.49	2.14	0.227	0.225	0.25	-0.04	1.553	11.21
G26	3304182	-8397.94	1.16	0.97	1.53	0.347	0.319	0.53	-0.24	1.689	14.51
G27	3304157.9	-8698.93	0.47	1.1	1.73	0.301	0.289	0.41	-0.14	1.6	8.85
G28	3304833.5	-9139.62	0.25	1.6	2.23	0.227	0.213	0.39	-0.23	1.525	14.04
Cores											
C1-1	3305300	-7485.2	0.28	0.58	1.94	0.26	0.250	0.46	-0.13	1.58	16.4
C1-2			0	1.28	2.18	0.221	0.224	0.35	0.04	1.51	20.64
C1-3			0.27	1.76	2.23	0.213	0.203	0.43	-0.16	1.508	21.59
C1-4			0.32	1.8	2.08	0.237	0.210	0.56	-0.3	1.558	16.4
C1-5			0.18	1.4	1.89	0.269	0.248	0.61	-0.2	1.596	19.23
C1-6			0	1.64	2.39	0.191	0.186	0.39	-0.1	1.531	14.98
C1-7			0.72	1.16	1.93	0.263	0.228	0.65	-0.31	1.631	14.51
C1-8			0.1	1.31	2.27	0.208	0.199	0.42	-0.16	1.556	20.17
C1-9			0	2.84	2.42	0.196	0.187	0.44	-0.17	1.494	21.11
C1-10			0	2.6	2.14	0.226	0.218	0.48	-0.11	1.492	20.64
C1-11			0	1.76	2.07	0.238	0.218	0.53	-0.24	1.539	23.94
C1-12			8.63	1.87	2.17	0.222	0.203	0.48	-0.27	1.464	29.61
C1-13			0	1.72	2.02	0.247	0.233	0.51	-0.17	1.6	14.04

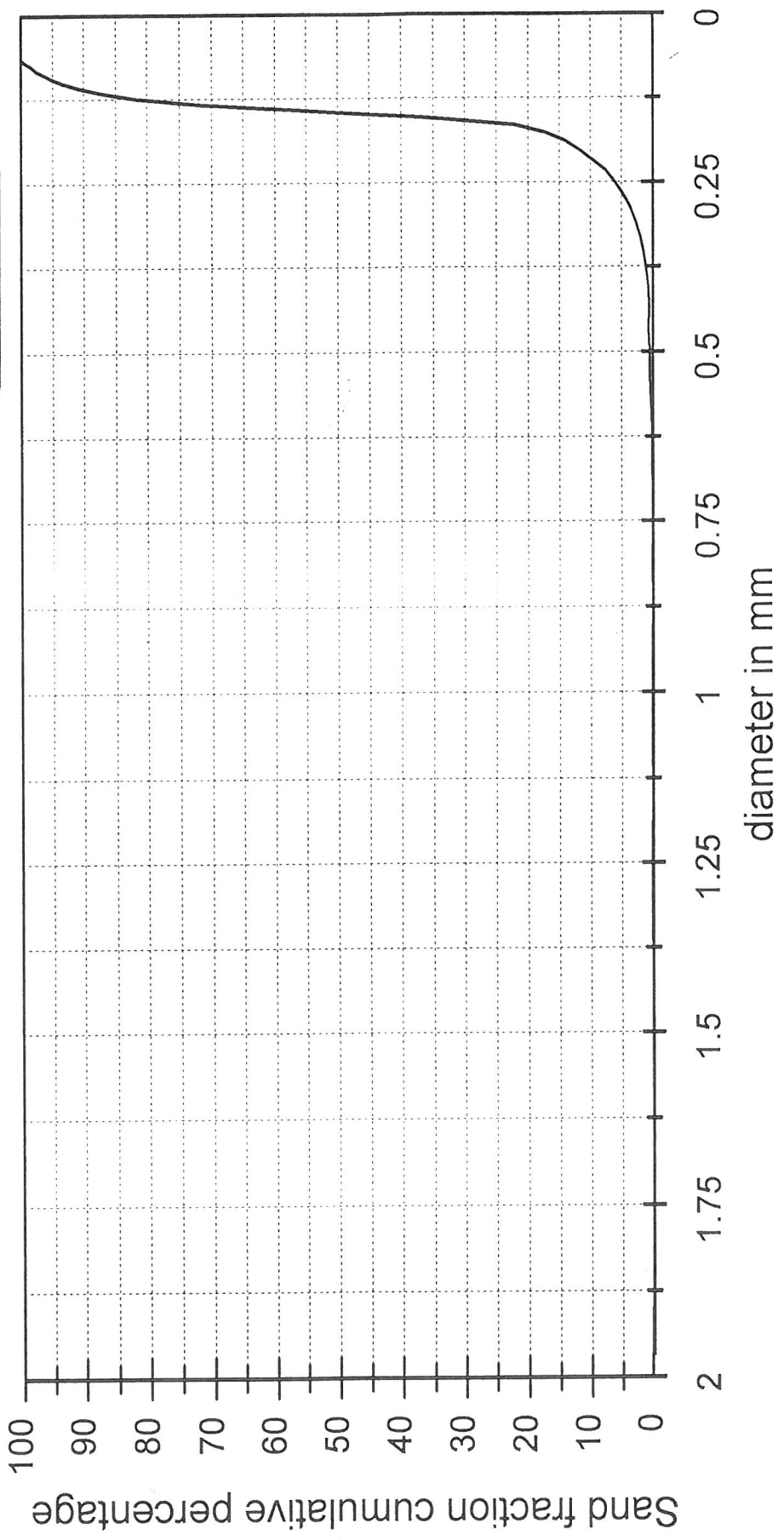
Sample No.	Lo 31 Coordinates		Gravel% (>2000µ)	Mud% (<63µ)	Graphics Statistics from Sand Fraction					Skewness	Dry Density (Tons/m3)	Carbonate %
	X	Y			Median	Mean	mm-Mn	mm-Med	Sorting			
C2-1	3304902	-7906.7	2.29	1.06	1.89	1.76	0.295	0.270	0.5	-0.26	1.612	14.51
C2-2			3.15	2.17	2.04	1.85	0.277	0.243	0.58	-0.32	1.605	15.93
C2-3			7.29	0.84	1.11	0.94	0.52	0.463	0.83	-0.2	1.72	17.81
C2-4			2.71	1.35	1.97	1.94	0.261	0.255	0.43	-0.08	1.647	13.57
C2-5			0.34	0.51	1.82	1.79	0.289	0.283	0.46	-0.07	1.638	14.98
C2-6			0	1.84	2.07	2.06	0.239	0.238	0.43	-0.01	1.599	13.57
C2-7			1.68	1.32	2.04	1.95	0.259	0.243	0.48	-0.18	1.663	18.76
C3-1	3304240	-8596.4	1.8	0.91	1.63	1.47	0.36	0.323	0.54	-0.3	1.625	12.62
C3-2			5.6	0.27	1.61	1.44	0.369	0.328	0.62	-0.28	1.718	14.04
C3-3			34.54	3.27	1.37	1.21	0.432	0.387	0.77	-0.21	1.76	32.91
C3-4			26.44	1.56	1.66	1.43	0.371	0.316	0.69	-0.34	1.779	27.25
C3-5			2.35	1.35	1.67	1.52	0.349	0.314	0.51	-0.3	1.681	14.98
C3-6			11.06	4.85	1.95	1.89	0.269	0.259	0.58	-0.09	1.617	18.76
C3-7			0	1.63	2.16	2.12	0.229	0.224	0.36	-0.09	1.554	9.32
C3-8			0	1.78	2.23	2.24	0.211	0.213	0.35	0.05	1.565	9.79
C3-9			0	1.67	2.09	2.05	0.242	0.235	0.38	-0.1	1.563	14.51
C3-10			2.2	1.01	1.78	1.71	0.305	0.291	0.41	-0.16	1.645	12.62
C4-1	3301736	-6815.4	0.36	3.51	2.8	2.72	0.152	0.144	0.37	-0.22	1.444	23
C4-2			1.47	3.57	2.76	2.61	0.163	0.148	0.39	-0.38	1.49	22.53
C4-3			8.35	2.97	2.74	2.54	0.172	0.150	0.43	-0.46	1.628	32.44
C4-4			0.37	2.63	2.78	2.73	0.151	0.146	0.28	-0.19	1.481	27.25
C4-5			0.12	2.28	2.82	2.8	0.143	0.142	0.27	-0.07	1.461	28.19
C4-6			0	2.2	2.91	2.93	0.132	0.133	0.21	0.07	1.391	28.19
C4-7			0.25	3.23	2.93	2.93	0.131	0.131	0.22	-0.03	1.433	25.36
C5-1	3300589	-6489.1	0.89	2.99	2.86	2.88	0.136	0.138	0.26	0.08	1.382	26.3
C5-2			0.45	2.31	2.78	2.65	0.159	0.146	0.39	-0.32	1.516	22.53
C5-3			0.51	2.98	2.67	2.58	0.168	0.157	0.41	-0.22	1.527	24.42
C5-4			4.55	1.24	2.73	2.63	0.161	0.151	0.35	-0.28	1.49	27.72
C5-5			1.99	2.38	2.94	2.95	0.13	0.130	0.22	0.03	1.439	23.47
C5-6			0.57	2.29	2.86	2.6	0.165	0.138	0.49	-0.53	1.488	20.64
C5-7			0	2.47	2.85	2.76	0.147	0.139	0.37	-0.24	1.459	17.34
C5-8			7.99	1.92	2.65	2.28	0.205	0.159	0.73	-0.51	1.612	24.42
C5-9			14.04	0.73	1.32	1.19	0.438	0.401	0.88	-0.14	1.818	34.32

APPENDIX 2

CUMULATIVE FREQUENCY DISTRIBUTION CURVES

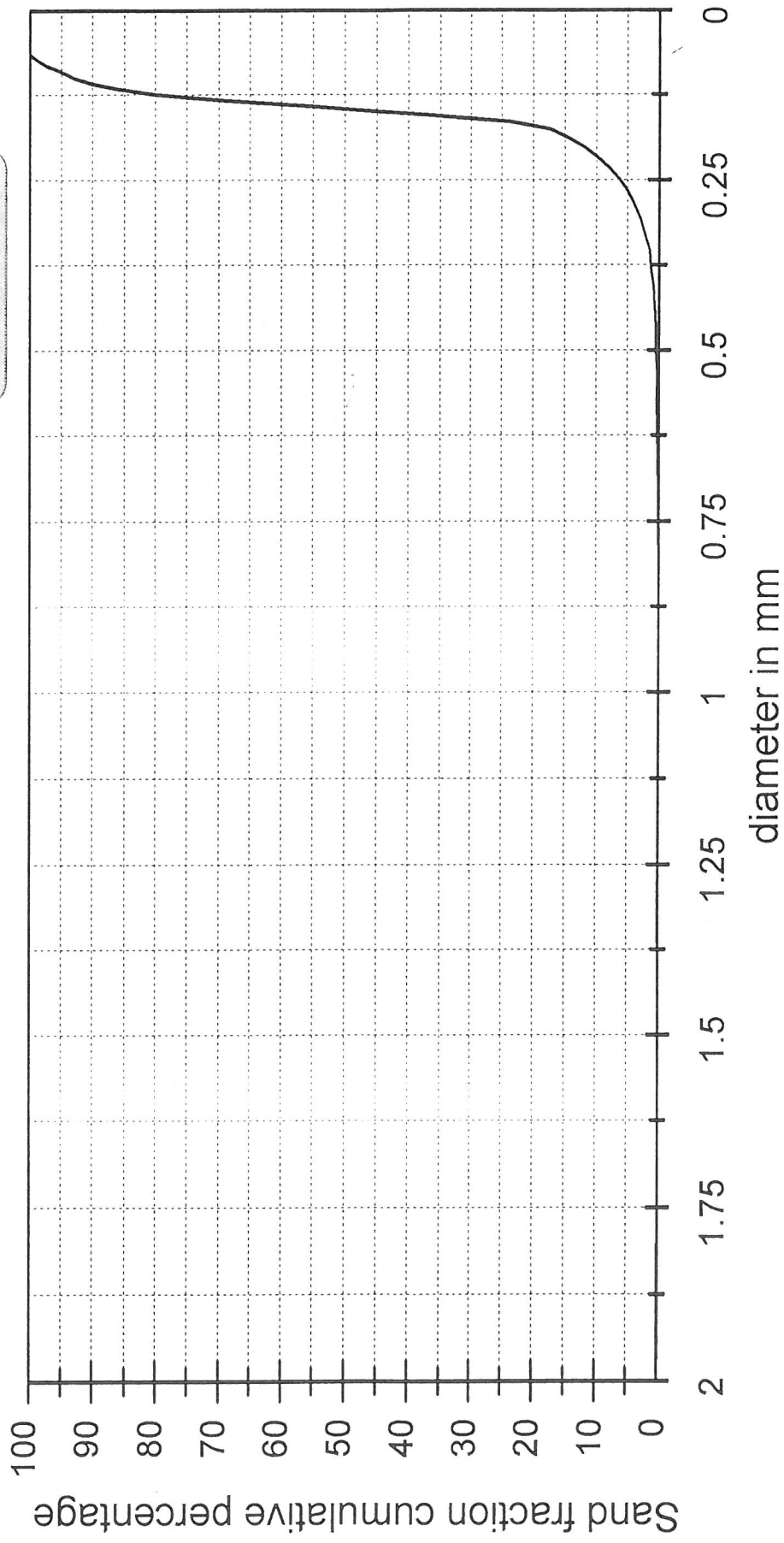
Sample Number G1

Gravel % = 0
Mud % = 1.87



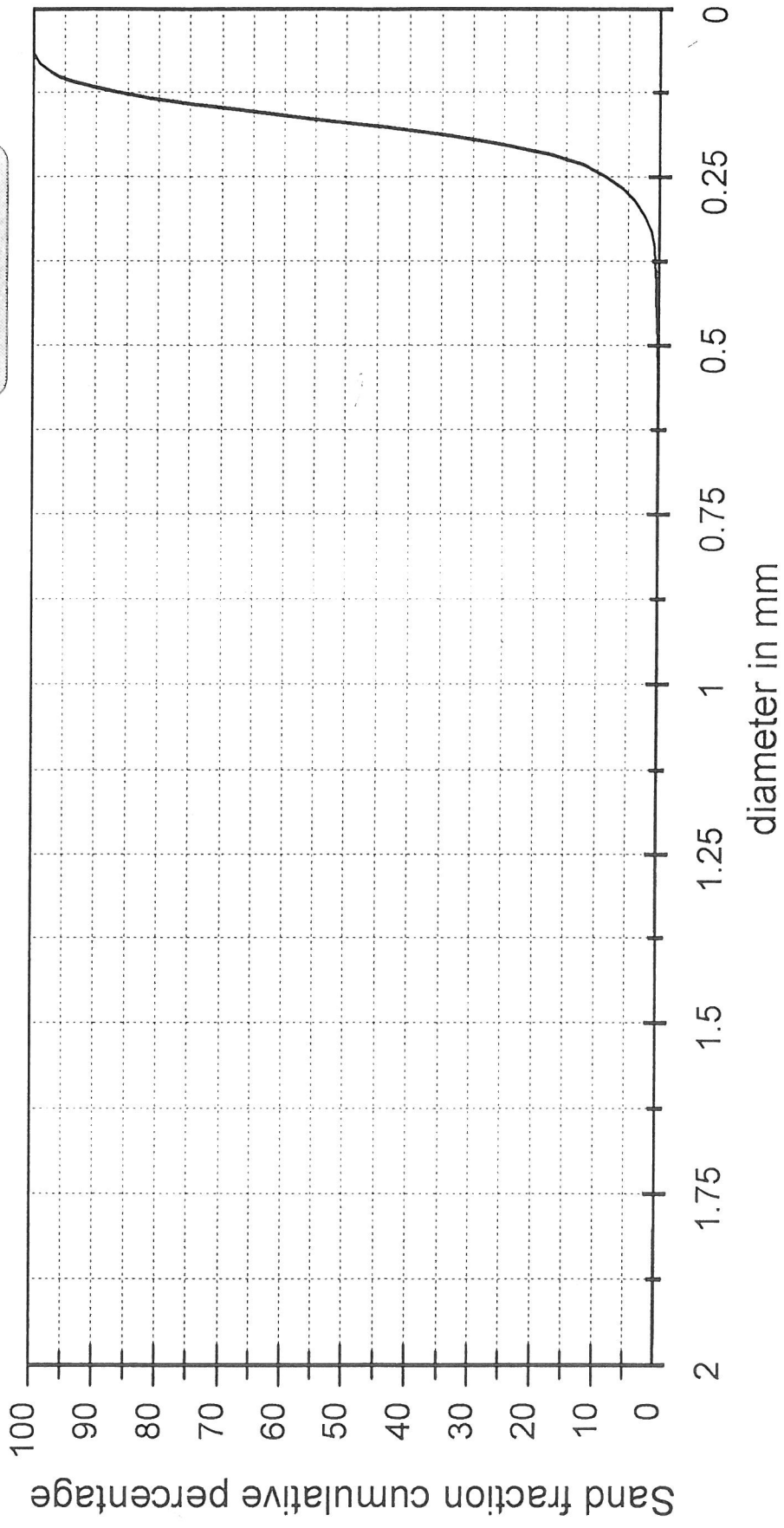
Sample Number G2

Gravel % = 0.34
Mud % = 2.39



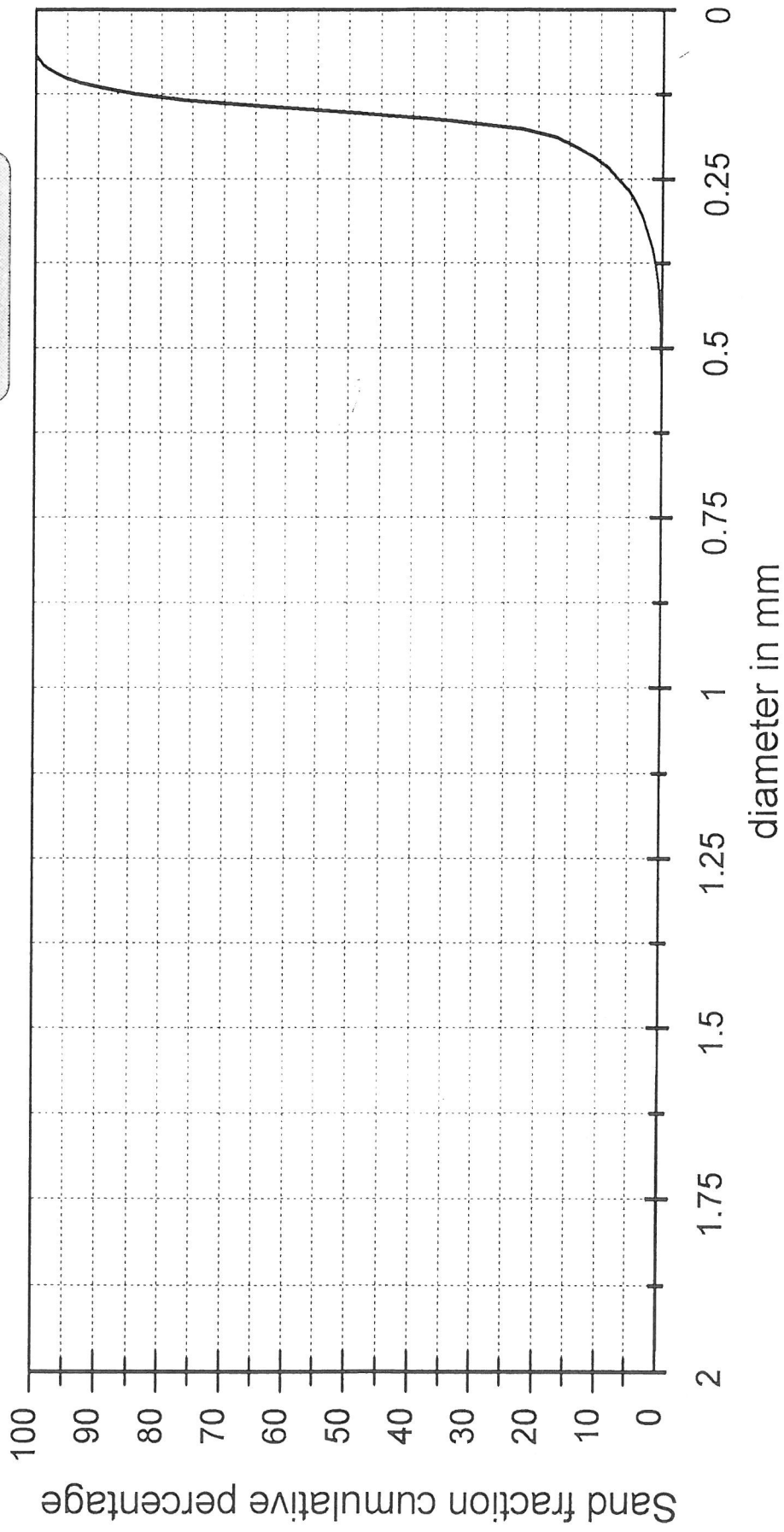
Sample Number G3

Gravel % = 0
Mud % = 1.88



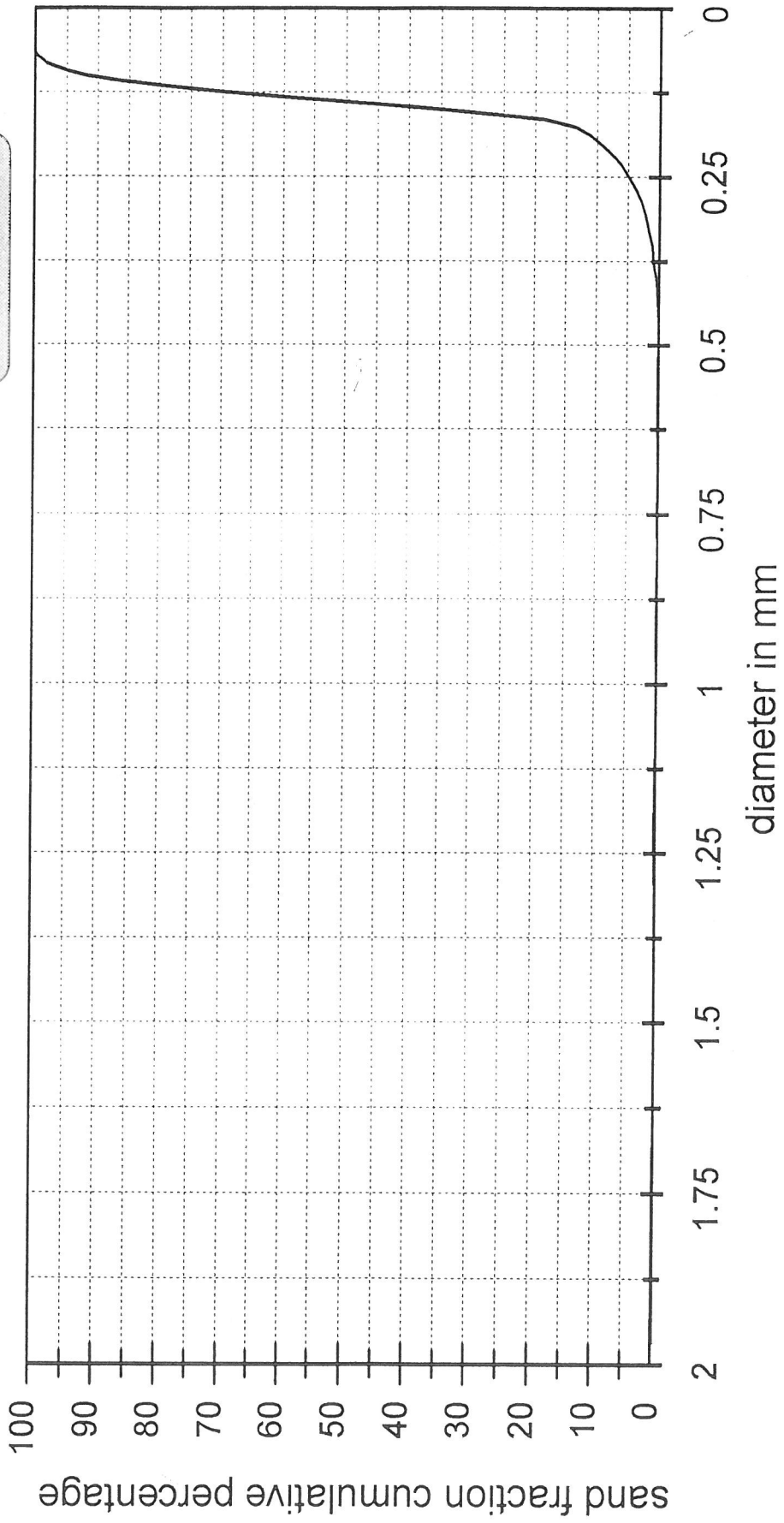
Sample Number G4

Gravel % = 0
Mud % = 2.26



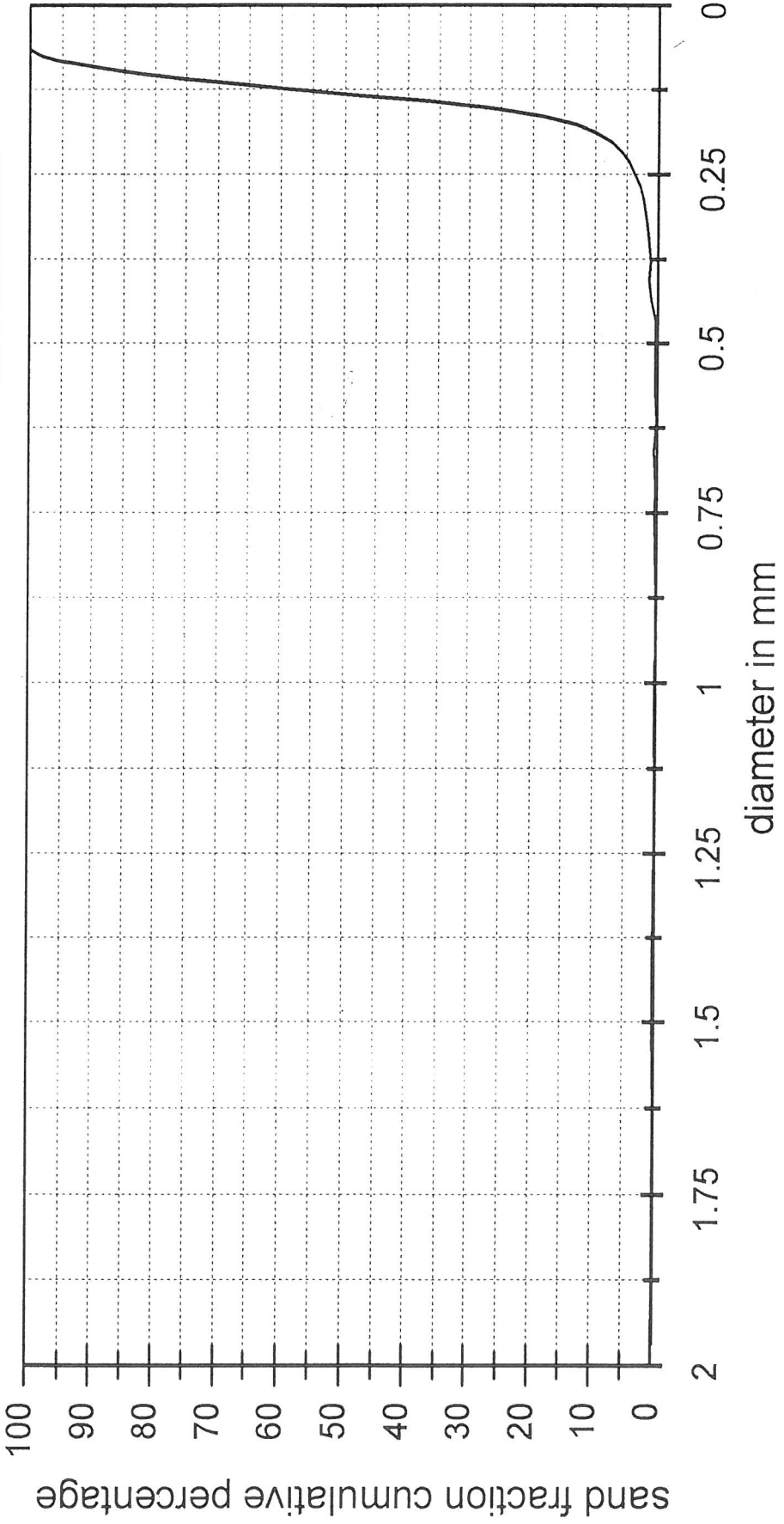
Sample Number G5

Gravel % = 0
Mud % = 2.17



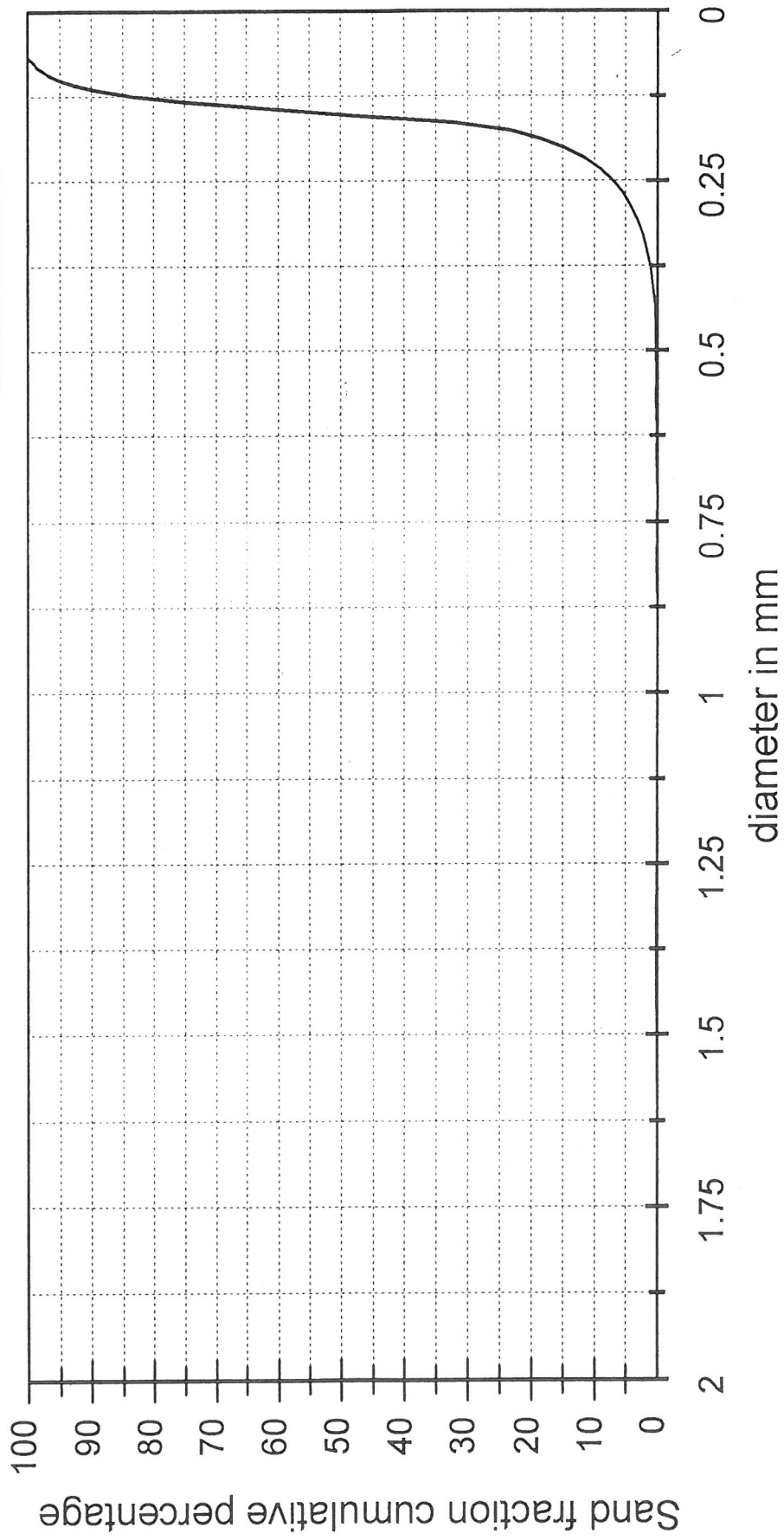
Sample Number G6

Gravel % = 0.16
Mud % = 2.62



Sample Number G7

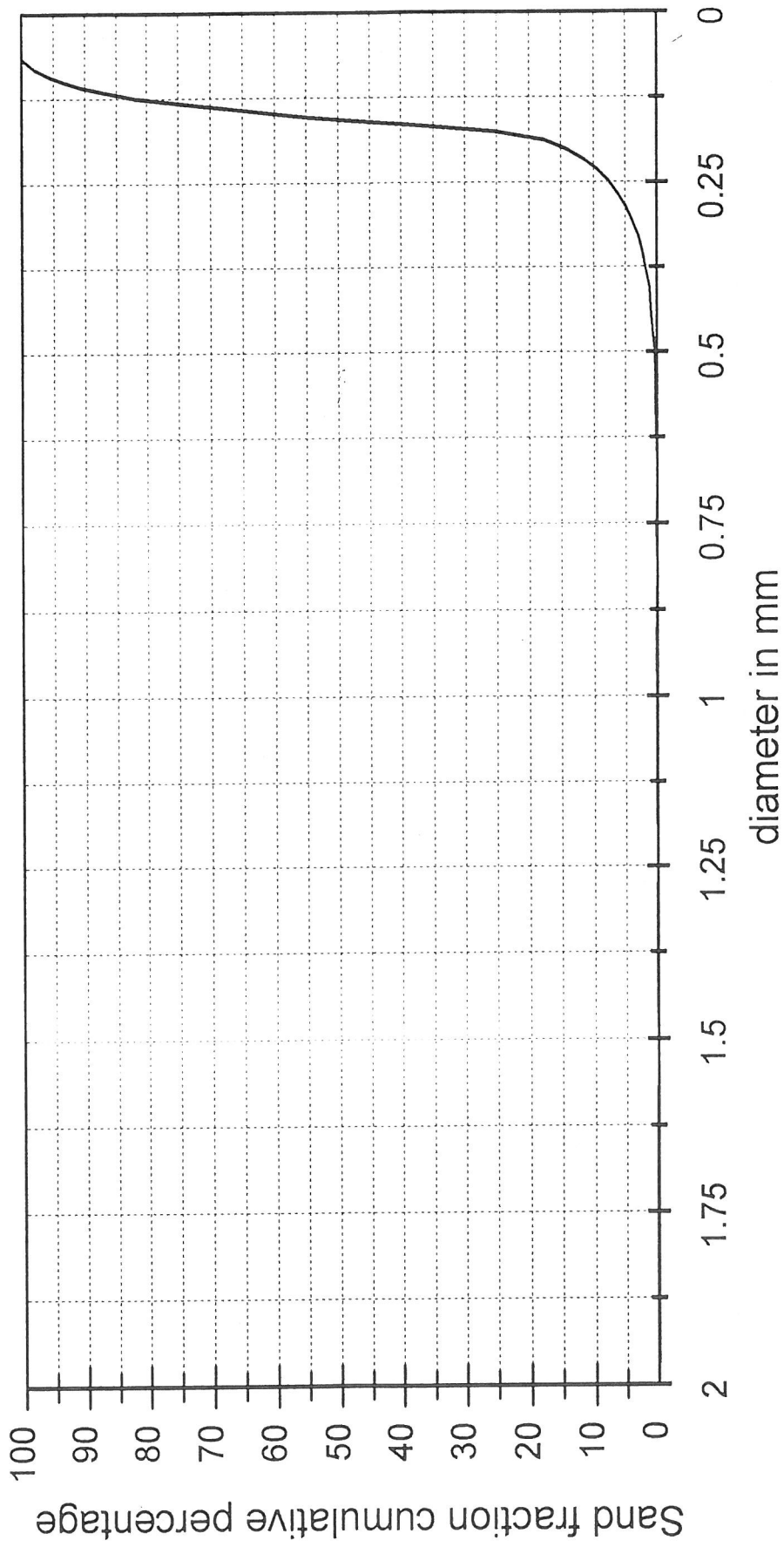
Gravel % = 0
Mud % = 1.85



0% coarse sand
7% medium sand
93% fine sand

Sample Number G8

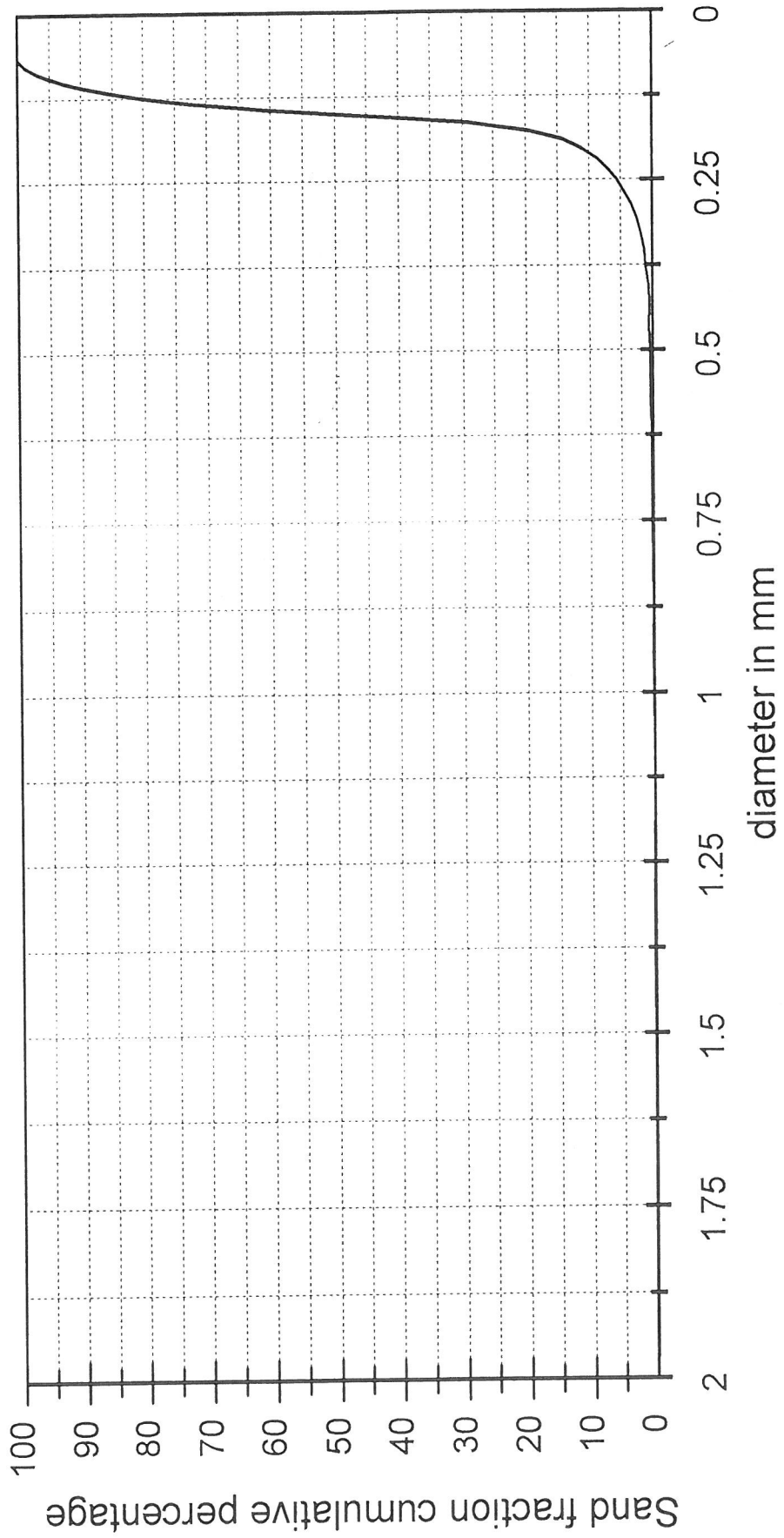
Gravel % = 0
Mud % = 1.84



0% coarse sand
8% medium sand
92% fine sand

Sample Number G9

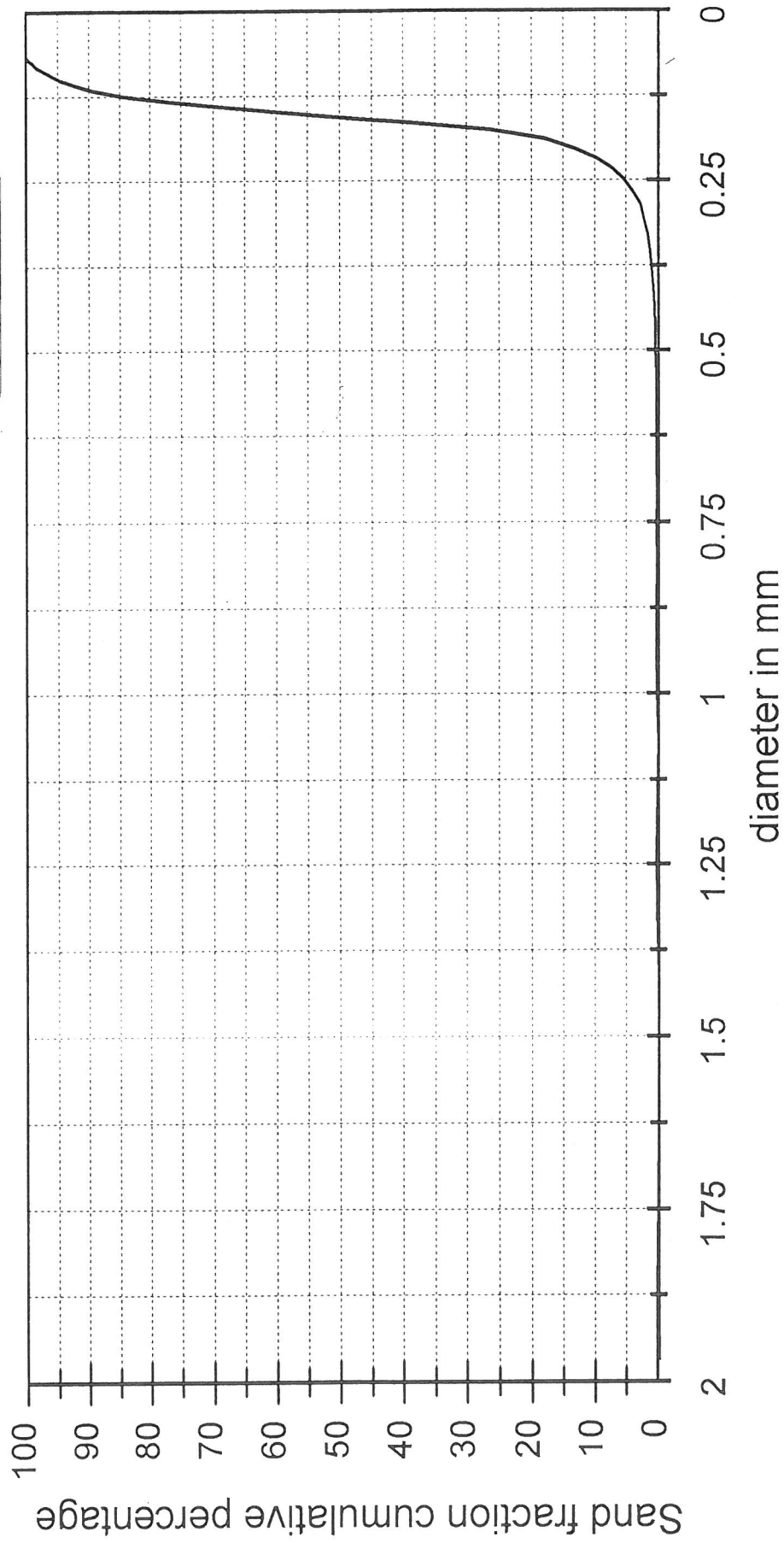
Gravel % = 0
Mud % = 1.85



0% coarse sand.
5% medium sand.
95% fine sand.

Sample Number G10

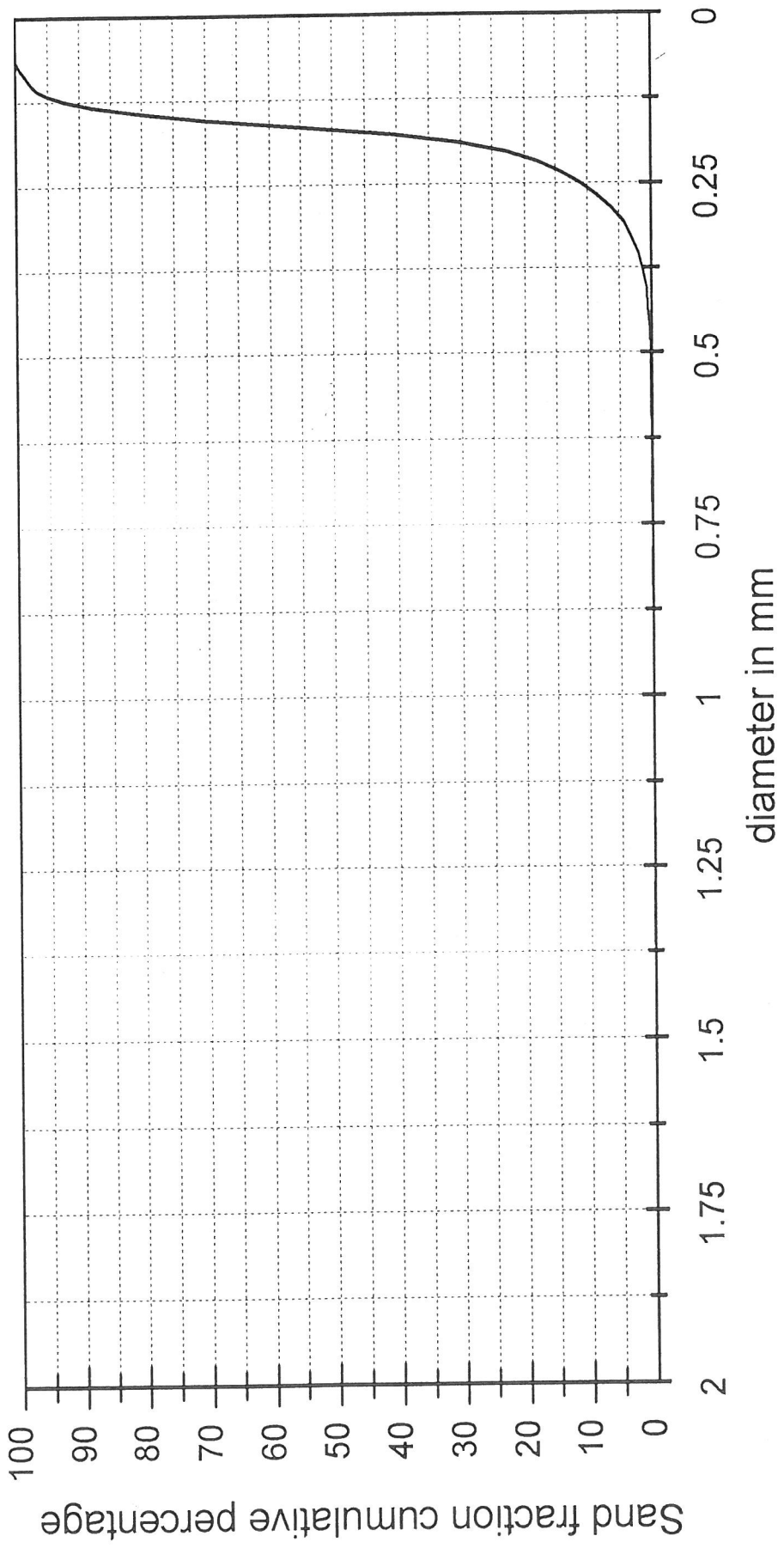
Gravel % = 0
Mud % = 2.29



0% coarse sand
5% medium sand
95% fine sand

Sample Number G11

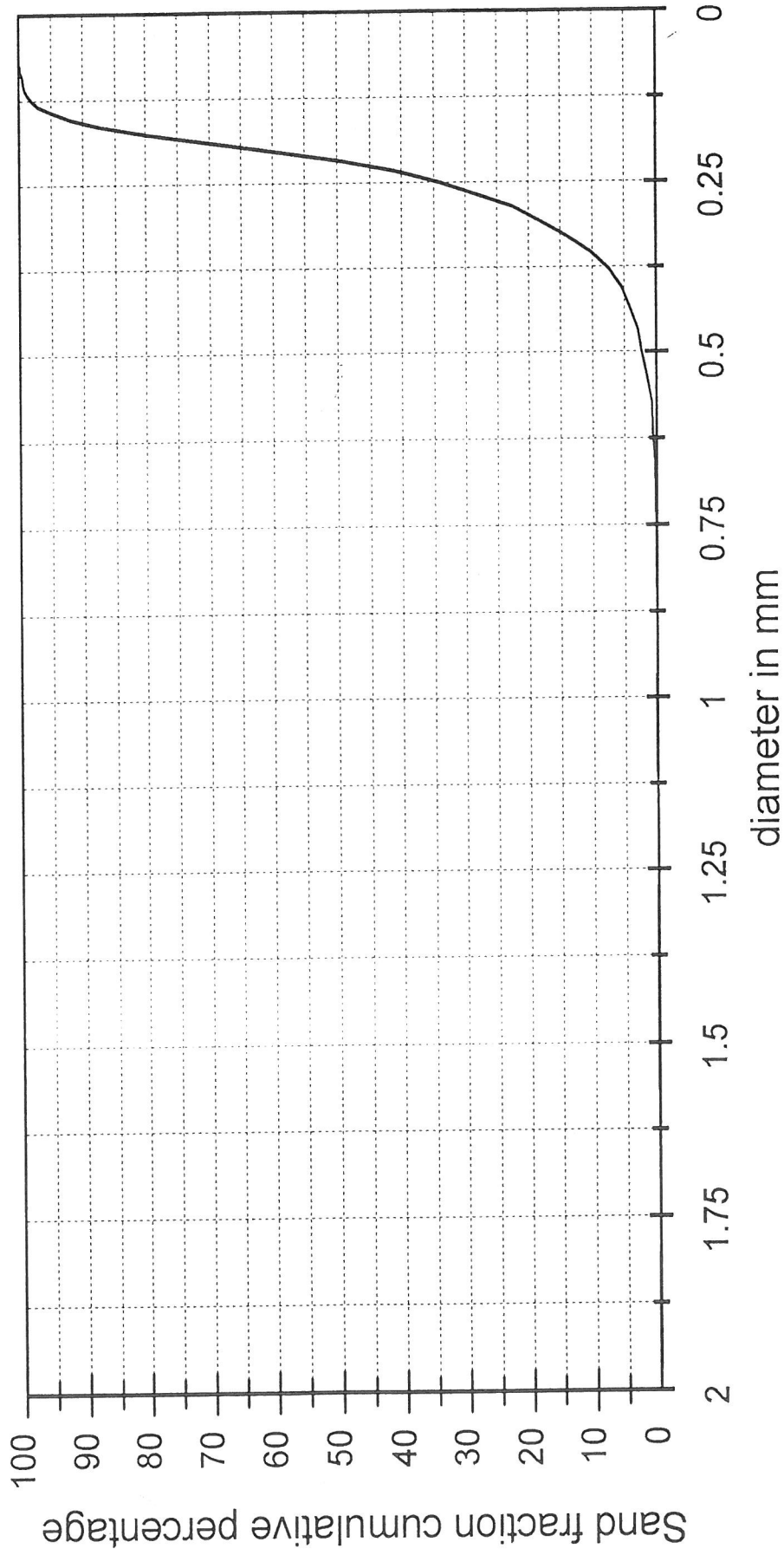
Gravel % = 0
Mud % = 1.98



0% coarse sand
1% medium sand
89% fine sand

Sample Number G12

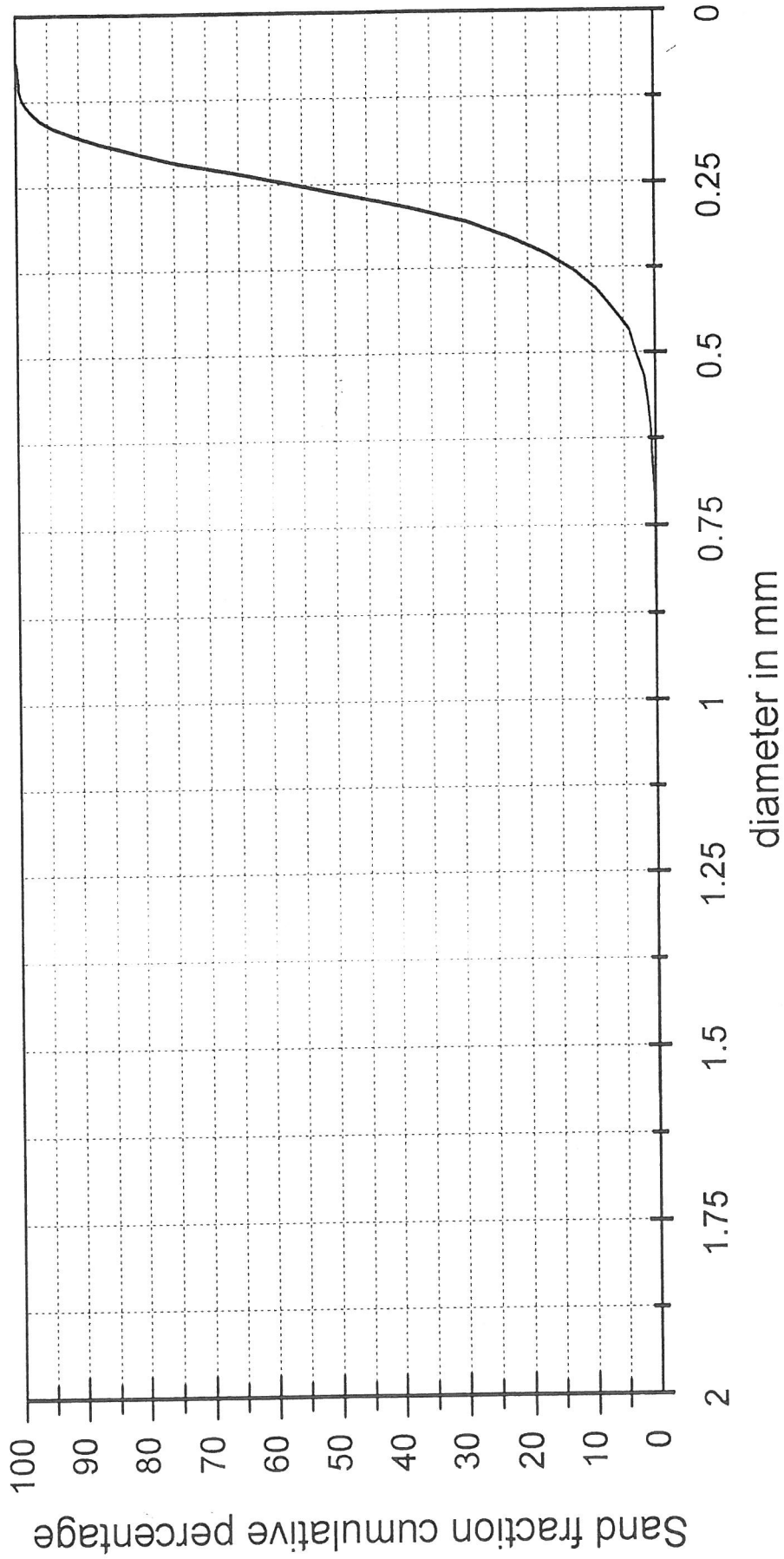
Gravel % = 0
Mud % = 1.44



1% coarse sand
36% medium sand
65% fine sand

Sample Number G13

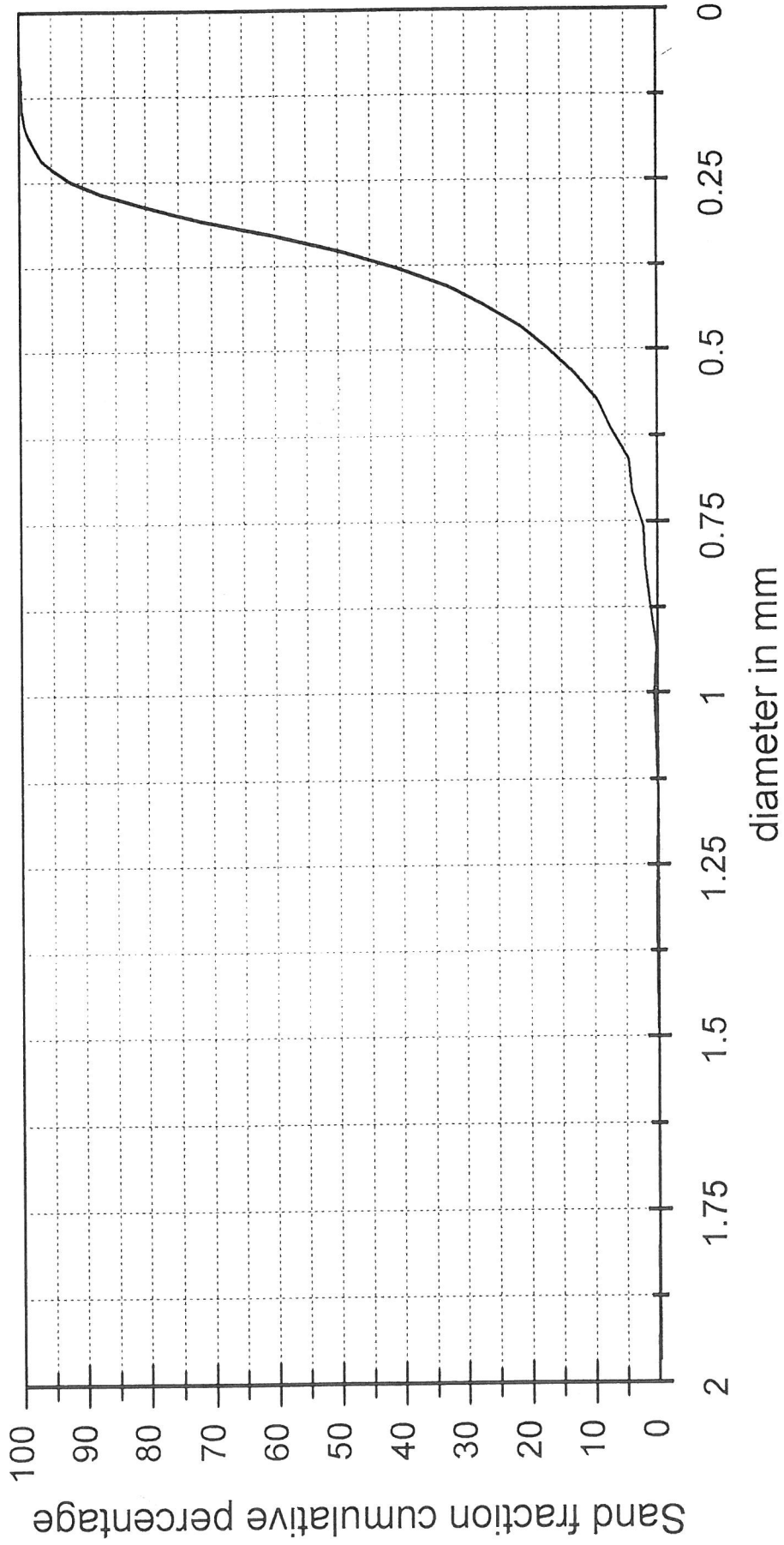
Gravel % = 0
Mud % = 1.64



*1% coarse sand,
54% medium sand,
45% fine sand*

Sample Number G14

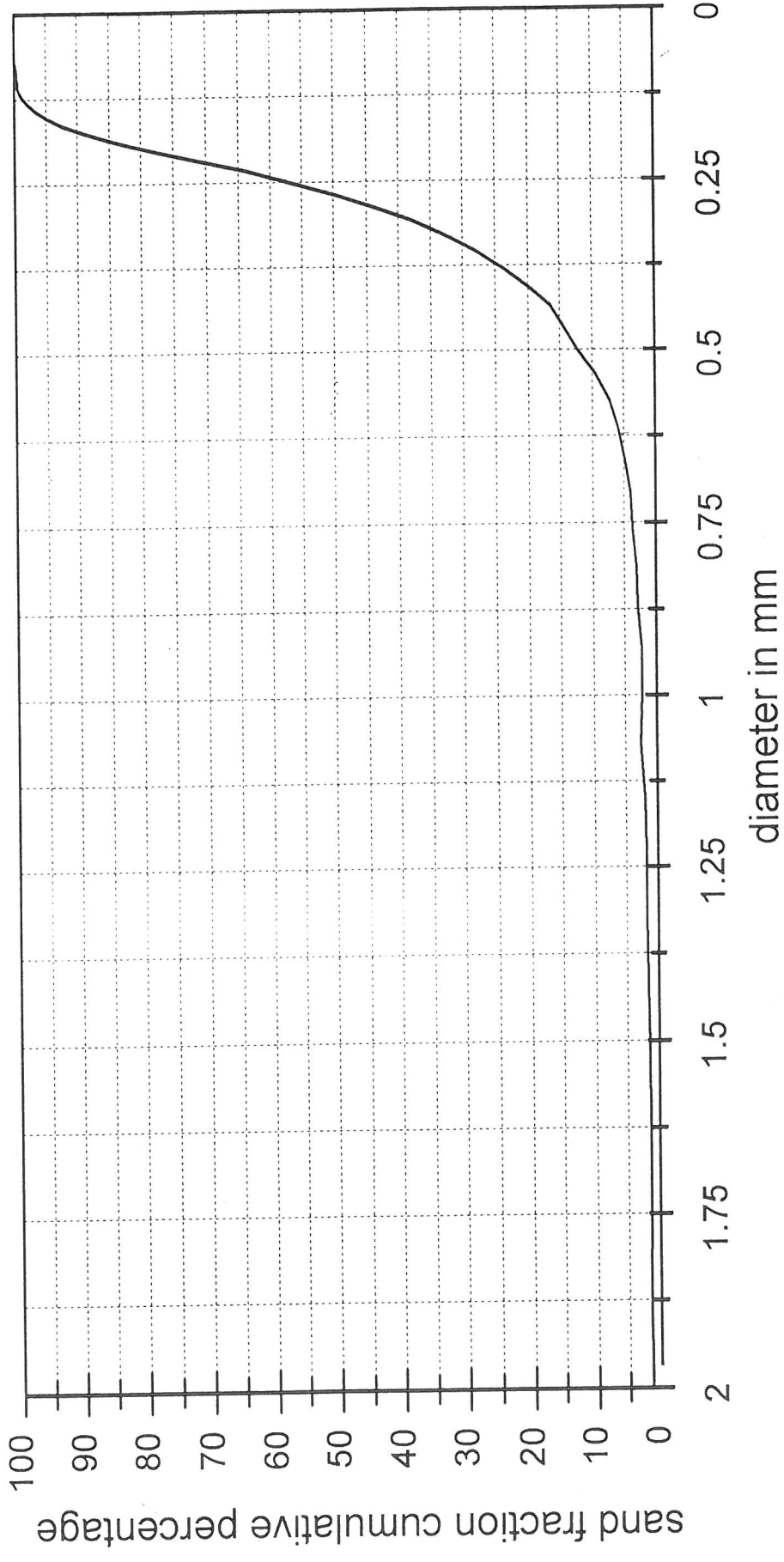
Gravel % = 1.15
Mud % = 1.07



7% coarse sand
85% medium sand
8% fine sand

Sample Number G15

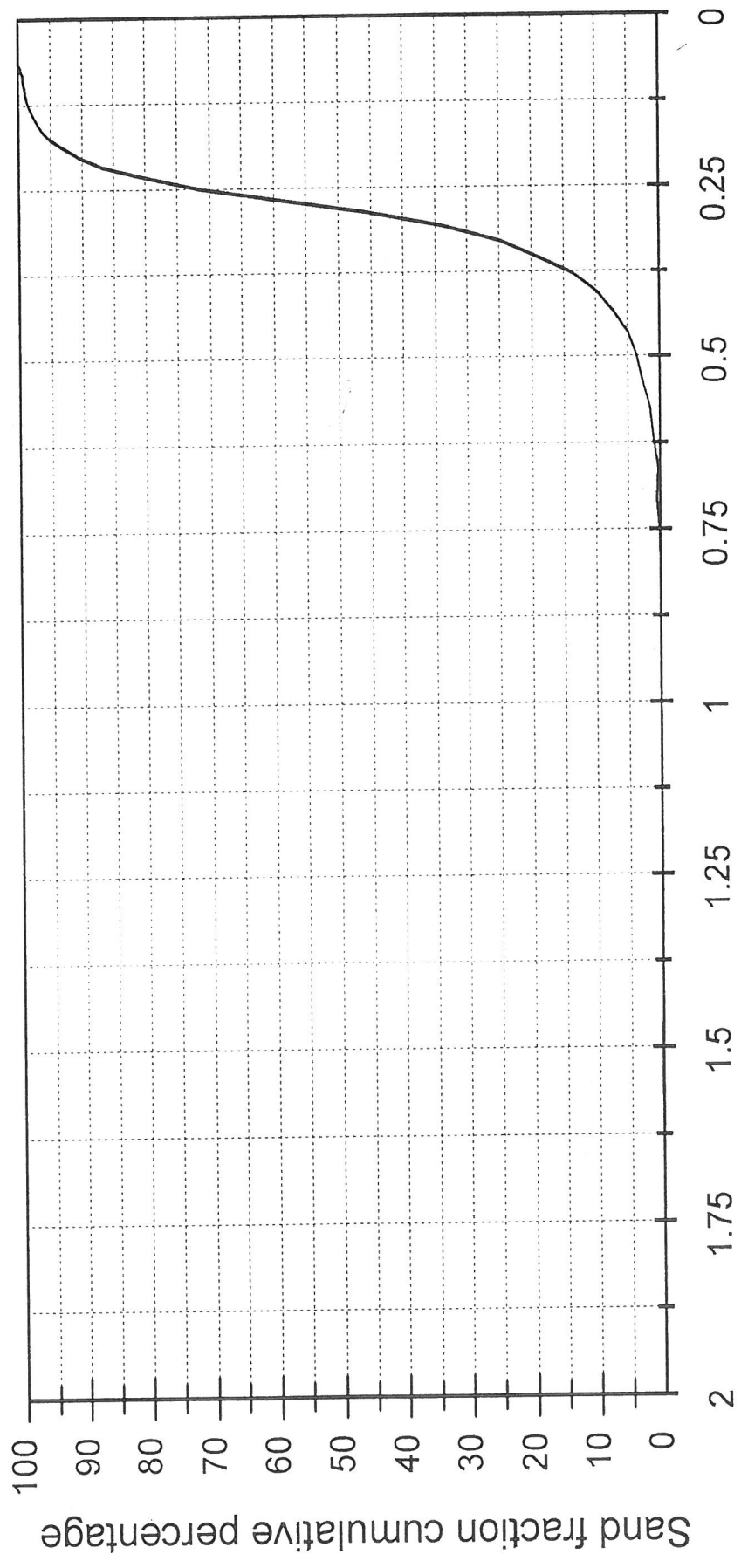
Gravel % = 1.04
Mud % = 1.57



6% coarse sand *
52% medium sand
42% fine sand

Sample Number G16

Gravel % = 0
Mud % = 1.75



diameter in mm

1% coarse sand.
69% med. sand.
30% fine sand